OPERATING MANUAL

ROCKLAND

MODELS 452 & 852 DUAL HI/LO FILTERS



Rockland Systems Corporation

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MODELS 452 & 852

DUAL HI/LO FILTERS

ROCKLAND SYSTEMS CORPORATION

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SECTION I

GENERAL INFORMATION

1-1. INTRODUCTION

The Models 452 and 852 are versatile dual-channel filters consisting of two identical channels in a common cabinet. Each filter channel has separate input/output terminals, offers high pass and low pass functions, 0 dB and 20 dB gain, Butterworth and Linear Phase responses and 3-digit resolution for cutoff frequency selection.

Individual channels may be readily interconnected for series or parallel operation, resulting in bandpass (or doubled rolloff) and band reject functions respectively.

Each filter channel provides switch selectable Flat Amplitude (Butterworth) response and Flat Delay (Linear Phase) response.

The Butterworth filter has maximally-flat amplitude response suitable for frequency-domain applications. Its cutoff frequency (fc) is defined as the frequency at which the amplitude response is down 3 dB.

The Linear Phase filter approximates a constant time delay for frequencies below its cutoff frequency. This filter is suitable for time-domain applications because of its inherent ability to pass transient waveforms with a very small amount of distortion and overshoot.

Models 452 and 852 are electrically and mechanically similar, covering the cutoff frequency range of 0.1 Hz to 111 KHz. Rolloff of the Model 452 is 24 dB/octave/channel, Model 852 is 48 dB/octave/channel. Factory-installed Option -01 extends cutoff frequency range and resolution on both models to 0.01 Hz.

Frequency-determining passive elements of the filters consist of stable precision metal film resistors and close tolerance polycarbonate or mica film capacitors. The active elements are FET-input IC operational amplifiers which provide highly stable gain, and very low noise and distortion. This combination of active and passive elements produces a filter having high cutoff frequency accuracy and resettability, and excellent temperature and long term stability. Another result of precise control of frequency-determining elements is close amplitude and phase match between channels.

1-2. DESCRIPTION

ELECTRICAL. Models 452 and 852 operate from either 115 or 230 volts ac, 50-500 Hz, and consume less than 5 watts of power. A rear-panel slide switch selects the nominal line voltage. The case of the instrument is grounded through the power cord, but signal ground can be isolated from power ground (through a 0.01 uf capacitor) via a rear-panel slide switch.

Cutoff frequency of each channel is selected via three 11-position (0-10) switches and a 4-position multiplier switch. The two pilot lights also serve as cutoff frequency decimal point indicators. Passband Gain of 0 dB or 20 dB may be selected for each channel. High Pass or Low Pass mode is individually selectable for each channel, as well as Flat Amplitude or Flat Delay response.

MECHANICAL. The instrument cabinet is 3.5 inches high by 17 inches wide (19 inches wide including rack mounts). It is 13 inches deep and weighs 10 pounds (Model 452) or 12 pounds (Model 852).

The power switch, operating controls, and input and output terminals are located on the front panel. The rear panel contains duplicate (parallel) input and output terminals for each channel, power connector, the fuse holder, the 115/230 Vac line selector switch, and a switch to disconnect signal ground from the power ground.

In its standard configuration the instrument is supplied in a cabinet suitable for table-top use, with feet and tiltstand. A rack-mount configuration is also available (See Options).

1-3. OPTIONS

The following options are available for both models:

Option -01: Extends low frequency range and resolution to 0.01 Hz.

Option -02: Provides 600-ohm nominal output impedance instead of 50 ohms.

Option -03: The instrument is shipped from the factory in a rack-mount

configuration without feet and tiltstand.

Option -04: A field-installable conversion kit, supplied in addition to the

standard configuration. It enables the user to convert the

instrument to rack-mount configuration.

1-4. SPECIFICATIONS, MODEL 452 & 452-01

FUNCTIONS

Each Channel:

Low Pass (DC Coupled) with 24 dB/oct

rolloff

High Pass with 24 dB/oct rolloff

Two Channels connected in series:
Identical cutoff frequencies
Identical cutoff frequencies
One channel High Pass,

Low Pass with 48 dB/oct rolloff High Pass with 48 dB/oct rolloff

one channel Low Pass
Two channels connected in parallel:

Band Pass with 24 dB/oct rolloffs
Band Reject: Broadband with 24 dB/oct
rolloff, or Sharp Notch Response

CUTOFF FREQUENCY RANGE & RESOLUTION

Frequency Settings:

Three 11-position switches (0, 1, 2, 3, 4, 5, 6, 7, 8, 9, 10) and a four-position (x10, x100, x1K, x10K) multiplier switch. Option -01 adds a fifth position (x1) to the multiplier switch.

Frequency Range:

With Option -01

Multiplier	Frequency (Hz)	Resolution (Hz)
×l	0.01-11.1	0.01
×10	0.1-111	0.1
×1 00	1-1.11K	1
×1K	10-11.1K	10
×10K	100-111K	100

FLAT AMPLITUDE (BUTTERWORTH) RESPONSE

Passband Gain:

Low Pass: 0 dB/20 dB, ± 0.25 dB. High Pass: 0 dB/20 dB, ± 0.25 dB,

(±0.5 dB in x 10K Multiplier position);

- 3dB at approximately 2 MHz.

Band Pass: Depends on separation of cutoff frequencies. If separation is more than two octaves, the Low Pass & High Pass specifications apply. If Low Pass & High Pass cutoffs are identical, an insertion loss of approx. 6 dB is produced; the 3 dB bandwidth extends from 0.8 fc to 1.25 fc and is equal to 0.45 fc. Band Reject & Sharp Notch: An insertion loss of approximately 6 dB is produced.

1-4. SPECIFICATIONS, MODEL 452 & 452-01 - continued

FLAT AMPLITUDE (BUTTERW ORTH) RESPONSE - continued

Cutoff Frequency Accuracy: ± 2%

Attenuation at Cutoff: 3 dB

Stopband Attenuation Rate (Rolloff): 24 dB/octave, nominal

Maximum Stopband Attenuation: 90 dB

Stability of Cutoff Frequency (Typical): ± 200 ppm/°C

Phase Match between Channels (Typical): 1° or 1%, whichever is greater

FLAT DELAY (LINEAR PHASE) RESPONSE

Low Pass Delay (Typical): $\frac{1}{2 f_c}$ seconds

Attenuation at Cutoff: Approx. 9 dB

Stability of Delay (Typical): ± 200 ppm/°C

Phase Match between Channels (Typical): 1° or 1%, whichever is greater

INPUT CHARACTERISTICS

Circuit: Single-ended, diode-protected

Impedance: 1 Megohm shunted by 50 pF

Full-scale Signal at 0 dB Gain: ± 10 Volts (7.1 V rms) DC to 300 KHz,

decreasing to ± 4 Volts (2.8 V rms) at 1 MHz

(Divide these by 10 at 20 dB Gain).

Absolute max. Input: ± 100 Volts

Max. DC component: High Pass: ± 100 Volts, 0 dB gain, ± 10 Volts,

20 dB gain

1-4. SPECIFICATIONS, MODEL 452 & 452-01 - continued

OUTPUT CHARACTERISTICS

Circuit:

Single-ended, short-circuit protected, may

be d-c isolated from power ground by rear

panel switch

Impedance:

50 ohms, nominal

Full-Scale Signal:

± 10 Volts (7.1 V rms) DC to 300 KHz,

decreasing to \pm 4 Volts (2.8 V rms) at 1 MHz

 $(R_1 \ge 5K)_t \pm 15 \text{ mA max. current}$

Broadband Noise at either Gain Setting:

100 microvolts rms max. for 100 KHz

detector bandwidth

Harmonic Components:

Input f = 1 KHz

90 dB below full-scale signal

A-C Line-related Spurious Components:

110 dB below full-scale signal *

DC Offset at 25° C:

Within 1 millivolt at any f_c setting

Drift vs. Temperature:

100 microvolts/°C typ, 500 microvolts/°C max.

Drift vs. Time (Typical):

100 microvolts/week

TYPICAL EQUIVALENT INPUT NOISE SPECTRAL DENSITY

At f = 10 Hz

f = 100 Hz

f≧1 KHz

100 nanovolts/ $\sqrt{\text{Hz}}$

60 nanovolts/√Hz

20 nanovolts/\(\sqrt{Hz}\)

GENERAL

Power Requirements:

 $115/230 \, \text{Vac} \pm 10\%$, 50-500 Hz, 5 watts

Operating Temperature:

0°C to + 50°C

Storage Temperature:

-20°C to + 70°C

Connectors:

BNC's on front & rear panel

Floating Operation:

Slide switch on rear panel to disconnect

circuit ground from power ground.

^{*} Derate specification by 6 dB for Model 452-01 when operating in its optional range (x1)

1-4. SPECIFICATIONS, MODEL 452 & 452-01 - continued

GENERAL - continued

Size: 3-1/2" H x 17" W x 13" D (8.9 cm x 43.2 cm

 \times 33 cm)

Weight: 10 lbs. (4.5 Kg) Net, 14 lbs. (6.5 Kg) Shippin

Configuration: Bench-Top, convertible to rack-mount

Accessories supplied: 2 Instruction Manuals

1-5. SPECIFICATIONS, MODEL 852 & 852-01

FUNCTIONS

Each Channel: Low Pass (DC Coupled) with 48 dB/oct rolloff

High Pass with 48 dB/oct rolloff

Two Channels connected in series:

(Identical cutoff frequencies)

Low Pass with 96 dB/oct rolloff
(Identical cutoff frequencies)

High Pass with 96 dB/oct rolloff

(One channel High Pass,

one channel Low Pass)

Band Pass with 48 dB/oct rolloff
Two channels connected in parallel:

Band Reject with 48 dB/oct rolloff

CUTOFF FREQUENCY RANGE & RESOLUTION

Frequency Settings: Three 11-position switches (0, 1, 2, 3,

4, 5, 6, 7, 8, 9, 10) and a four-position (x10, x100, x1K, x10K) multiplier switch. Option -01 adds a fifth posotion (x1) to

the multiplier switch.

Frequency Range: Multiplier Frequency (Hz) Resolution (Hz)

With Option -01 0.01-11.1 0.01 χl x10 0.1-111 0.1 ×100 1-1.11K 1 x1K 10-11.1K 10 ×10K 100-111K 100

1-5. SPECIFICATIONS, MODEL 852 & 852-01 - continued

FLAT AMPLITUDE (BUTTERWORTH) RESPONSE

Passband Gain: Low Pass: 0 dB/20 dB, $\pm 0.5 dB$.

High Pass: 0 dB/20 dB, $\pm 0.5 dB$,

(± 1 dB in x 10K Multiplier position);

- 3 dB at approximately 1 MHz.

Band Pass: Depends on separation of cutoff frequencies. If separation is more than two octaves, the Low Pass & High Pass specifications apply. If Low Pass & High Pass cutoffs are identical, an insertion loss of approx. 6 dB is produced; the 3 dB bandwidth extends from 0.9 f_c to 1.12 f_c and is equal to 0.22 f_c. Band Reject: An insertion loss of approximately

6 dB is produced.

Cutoff Frequency Accuracy: ± 2%

Attenuation at Cutoff: 3 dB

Stopband Attenuation Rate (Rolloff): 48 dB/octave, nominal

Maximum Stopband Attenuation: 90 dB

Stability of Cutoff Frequency (Typical): ± 200 ppm/°C

Phase Match between Channels (Typical): 2° or 2%, whichever is greater

FLAT DELAY (LINEAR PHASE) RESPONSE

Low Pass Delay (Typical): $\frac{1}{f_c}$ seconds

Attenuation at Cutoff: Approx. 17 dB

Stability of Delay (Typical): ± 200 ppm/°C

Phase Match between Channels (Typical): 2° or 2%, whichever is greater

INPUT CHARACTERISTICS

Circuit: Single-ended, diode-protected

Impedance: 1 Megohm shunted by 50 pF in 0 dB Gain,

shunted by 75 pF in 20 dB Gain

1-5. SPECIFICATIONS, MODEL 852 8 852-01 - continued

INPUT CHARACTERISTICS - continued

Full-Scale Signal at 0 dB Gain: ± 10 Volts (7.1 V rms) DC to 300 KHz,

decreasing to ± 4 Volts (2.8 V rms) at 1 MHz (Divide these by 10 at 20 dB Gain).

Absolute max. Input: ± 100 Volts

Max. DC component: High Pass: $\pm 100 \text{ Volts}$, 0 dB gain, ± 10

Volts, 20 dB gain

OUTPUT CHARACTERISTICS

Circuit: Single-ended, short-circuit protected, may

be d-c isolated from power ground by rear panel

switch

Impedance: 50 ohms, nominal

Full-Scale Signal: ± 10 Volts (7.1 V rms) DC to 300 KHz,

decreasing to \pm 4 Volts (2.8 V rms) at 1 MHz

 $(R \ge 5 \text{ K})$, $\pm 15 \text{ mA max. current}$

Broadband Noise at either Gain Setting: 200 microvolts rms max. for 100 KHz detector

bandwidth

Harmonic Components:

Input f = 1 KHz 80 dB below full-scale signal

A-C Line-related Spurious Components: 100 dB below full-scale signal *

DC Offset at 25°C: Within 5 millivolts at any f_c setting

Drift vs. Temperature: 300 microvolts/°C typ, 1.5 millivolts/°C max.

Drift vs. Time (Typical): 500 microvolts/week

TYPICAL EQUIVALENT INPUT NOISE SPECTRAL DENSITY

At f = 10 Hz 250 nanovolts/ $\sqrt{\text{Hz}}$ f = 100 Hz 100 nanovolts/ $\sqrt{\text{Hz}}$ $f \ge 1 \text{ KHz}$ 40 nanovolts/ $\sqrt{\text{Hz}}$

^{*} Derate specification by 6 dB for Model 852-01 when operating in its optional range (x1)

1-5. SPECIFICATIONS, MODEL 852 & 852-01 - continued

GENERAL

Power Requirements:

 $115/230 \, \text{VAC} \pm 10\%$, $50-500 \, \text{Hz}$, 5 watts

Operating Temperature:

0°C to + 50°C

Storage Temperature:

-20°C to + 70°C

Connectors:

BNC's on front & rear panel

Floating Operation:

Slide switch on rear panel to disconnect

circuit ground from power ground.

Size:

3 1/2" H x 17" W x 13" D (8.9 cm x 43.2 cm x

33 cm)

Weight:

12 lbs. (5.5 Kg) Net, 15 lbs. (7 Kg) Shipping

Configuration:

Bench-Top, convertible to rack-mount

Accessories supplied:

2 Instruction Manuals

SECTION II

OPERATION

2-1. INTRODUCTION

The instrument is electrically operational as shipped from the factory. The following paragraphs describe inspection, power requirements, interconnection, and operation.

2-2. INSPECTION

This instrument was carefully inspected and tested prior to shipment. It was operated for a number of hours to reduce the probability of early failure. After unpacking the unit, inspect it carefully for shipping damage. Check especially for broken controls and connectors, and dented or scratched cabinet parts. Should the instrument show any signs of damage, file a claim with the carrier immediately. Preserve the carton and packing materials; they will be required by the carrier.

It is recommended that conformance to specifications be verified upon receipt. In case of discrepancies, refer to the warranty at the beginning of this manual.

2-3. INSTALLATION AND POWER REQUIREMENTS

Models 452 and 852 are designed for table-top operation or installation in a standard 19-inch RETMA rack. Ambient temperature within the rack must not exceed +50 °C while the instrument is operating. Other paragraphs in this section describe connections and switch settings which should be made before the unit is installed.

CAUTION

Always ensure that the 115/230 volt switch is set for the nominal line voltage and that a fuse of the proper rating is installed in the instrument. If the switch is set incorrectly or a fuse of the wrong rating is used, the instrument may be damaged or fail to operate.

The instrument will operate from either 115 or 230 volts ac, 50-500 Hz. Converstion for line voltage is performed with a slide switch mounted on the rear panel (see Figure 2-1). The unit is shipped with the switch set for 115 volts. To change the setting, insert a small-blade screwdriver in the switch slot and move switch to expose 115 for 115 Vac operation, or 230 for 230 Vac operation.

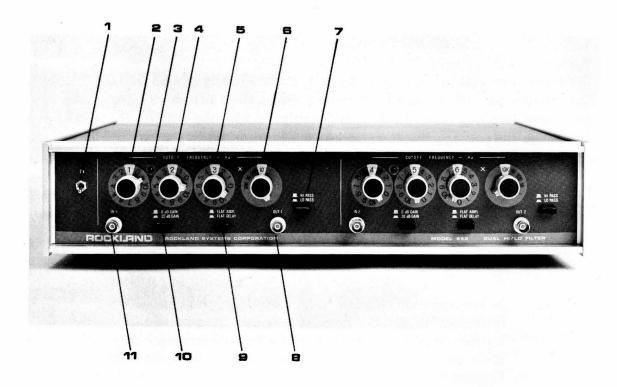
The instrument is shipped with a 1/4-amp slow-blow fuse for 115-volt or 230-volt operation.

WARNING

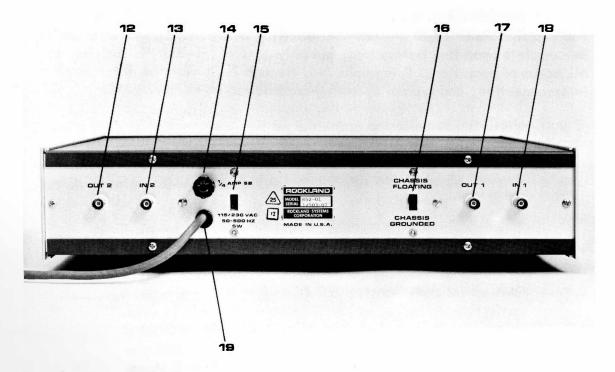
In keeping with standard safety practice, the case of the instrument is grounded through the power cord. If the instrument must be connected to a two-wire receptacle, use a parallel-ground adapter and connect the short lead to ground.

2-4. CONTROLS AND INDICATORS

Controls and indicators are shown in Figure 2-1 and described in Table 2-1. The descriptions in Table 2-1 and the following paragraphs are not intended to be complete operating instructions, but only general information applying to all modes of operation. Paragraphs 2-5, through 2-10 describe filter settings, interconnection, and typical operating procedures.



FRONT PANEL



REAR PANEL

Fig. 2-1. Controls and Indicators

Table 2-1. Controls and Indicators

NUMBER	DESCRIPTION
1	On Switch: The switch is moved to the on position to supply power to the instrument
-	Controls and Indicators numbered 2 through 11 pertain to Channel 1:
2	First significant digit of Cutoff Frequency setting, 0 – 10 positions, continuous rotation
3	A light-emitting diode (LED) indicates that power is on and also serves as a decimal point indicator for the Cutoff Frequency setting
4	Second significant digit of Cutoff Frequency setting, 0 – 10 positions, continuous rotation
5	Third significant digit of Cutoff Frequency setting, 0 – 10 positions, continuous rotation
6	Decimal Multiplier of Cutoff Frequency setting, 4 or 5 positions, depending on option
7	Low Pass (In) or High Pass (Out) selector switch
8	Output BNC Connector
9	Flat Delay (In) or Flat Amplitude (Out) selector switch
10	20 dB Gain (In) or 0 dB Gain (Out) selector switch
11	Input BNC Connector
- "	Channel 2 Controls and Indicators are identical to those of Channel 1
12	Channel 2 Output BNC Connector
13	Channel 2 Input BNC Connector

Table 2-1. Controls and Indicators

NUMBER		DESCRIPTION	
14		eholder for 1/4 Amp slow-blow fuse for er 115 V or 230 V operation	
15	115,	/230 V line voltage selector switch	
16		position switch: connects signal grour power (and chassis) ground, or floats sign und	
17	Cha	nnel 1 Output BNC Connector	
18	Cha	nnel 1 Input BNC Connector	
19	3-w	ire power cord	

2-5. INPUT SIGNAL

The maximum input signal amplitude (at 0 dB Gain) is specified as ±10 Volts (7.1 V rms) up to a frequency of 300 KHz. This is the signal amplitude which can be handled linearly by the instrument. Above 300 KHz the input signal handling capability is reduced as shown in Fig. 2-2. The reduction is due to Slew-Rate* limitations of the Operational Amplifiers employed in the instrument.

When 20 dB Gain is employed, the maximum input signal amplitude is ± 1.0 Volt (0.71 V rms) up to 300 KHz.

CAUTION

Input signals in excess of $\pm 100 \text{ V}$ in either Gain setting may damage the instrument.

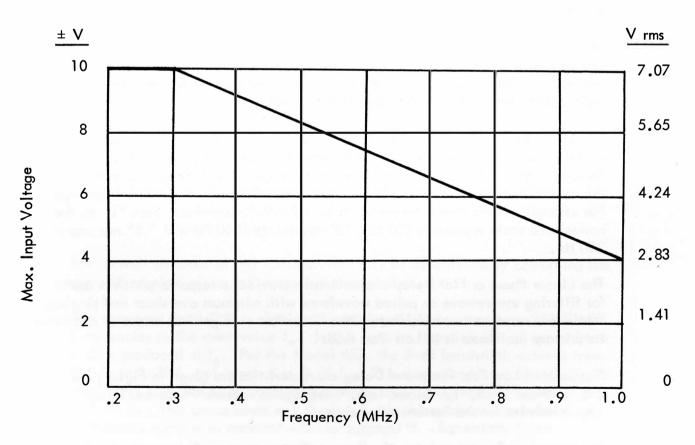


Fig. 2-2 Full-Scale Input Signal vs. Frequency

^{*} The term "Slew-Rate" refers to the ability of an Operational Amplifier to follow fast changes in input signal and it is usually expressed in volts/usec.

2-6. TYPICAL OPERATING PROCEDURES

a. Low-Pass or High-Pass Filter

The operating mode of each channel of the instrument is selected with the HI PASS/LO PASS switch. The position of this switch determines whether the channel is operating as a Low Pass (IN) or High Pass (OUT) filter.

In the Low Pass mode of operation the passband of the filter extends from DC to the cutoff frequency which is defined by the settings of the three CUTOFF FREQUENCY dials and the MULTIPLIER. In the High Pass mode of operation the passband extends from the cutoff frequency setting to the upper 3-dB point of the instrument (approximately 2 MHz for Model 452 and 1 MHz for Model 852).

b. Response Selection

The desired type of response for each channel is selected with the FLAT AMPL/FLAT DELAY switch. The position of this switch determines whether the response of the channel is a Butterworth response (OUT) or Linear Phase response (IN).

The Butterworth characteristic provides a maximally flat amplitude response which is 3 dB down at the cutoff frequency. Beyond the cutoff frequency the amplitude response rolls off at a rate of 24 dB/octave (80 dB/decade) for the Model 452 and 48 dB/octave (160 dB/decade) for the Model 852.

The Low-Pass or High-Pass Butterworth response for either model may be determined by scaling the normalized plots given in Figures 2-3, 2-4, 2-5 and 2-6. To determine the frequency response for a particular Cutoff Frequency setting, the normalized scale on these plots should be multiplied by the cutoff frequency. For example, if the cutoff frequency is set to 500 Hz Low-Pass, then "1" on the normalized scale represents 500 Hz, "2" represents 1000 Hz and ".5" represents 250 Hz.

The Linear Phase or Flat Delay characteristic provides a response which is useful for filtering squarewave or pulsed waveforms with minimum overshoot and ringing. While this response is available in either Low-Pass or High-Pass modes of operation, its primary usefulness is in Low-Pass mode.

Normalized Low Pass Phase and Delay characteristics are given in Figures 2–7, 2–8, 2–9 and 2–10. For comparison, these figures include Phase and Delay characteristics for the Butterworth response.

The procedure for determining the Phase or Delay response for a particular Cutoff Frequency from the normalized plots is the same as outlined for the amplitude response. The actual Delay in seconds is equal to the value obtained from the plot divided by the value of cutoff frequency.

c. Gain Selection

The passband gain of each channel is selected with the 0 dB GAIN/20 dB GAIN Switch. The position of this switch determines whether the channel is operating with 0 dB Gain (OUT), or 20 dB Gain (IN).

The 20 dB Gain position is useful when filtering low-level signals. Since output noise of the filter is independent of the gain position, a 20 dB effective improvement in dynamic range is achieved.

d. Band-Pass Filter

The two channels of the instrument, one in High-Pass and the other in Low-Pass mode, may be cascaded as shown in Fig. 2-11 to provide Band-Pass operation. Flat Amplitude (Butterworth) response should be utilized in both channels.

When channels are cascaded for Band-Pass operation, the input signal should be connected to the High-Pass channel (IN 1), and the output of this channel (OUT 1) should be connected to the input of the Low-Pass channel (IN 2). The output signal is available at OUT 2.

The passband in this configuration extends from the High-Pass Cutoff Frequency to the Low-Pass Cutoff Frequency setting. Maximum passband gain of 40 dB is available. If only 20 dB gain is desired, channel 1 should be set to 20 dB gain and channel 2 should be set to 0 dB gain.

CAUTION

Reversing the gain settings will increase the output noise of this configuration, because channel 2 will amplify the output noise of channel 1.

The overall response of this configuration may be determined by combining the normalized plots given in Figures 2-3 through 2-6.

The narrowest Band-Pass is obtained by setting High-Pass and Low-Pass Cutoff Frequencies to the same value f_o . In this case an insertion loss of approximately 6 dB is produced at f_o . For the Model 452, the 3-dB bandwidth extends from 0.8 f_o to 1.25 f_o and is equal to 0.45 f_o . This corresponds to a Q of 2.2. For the Model 852, the 3-dB bandwidth extends from 0.9 f_o to 1.12 f_o and is equal to 0.22 f_o . This corresponds to a Q of 4.5. In this mode of operation, both instruments operate as constant - Q, or constant % - Bandwidth filters.

e. Band-Reject Filter

The two channels of the instrument, one in High-Pass and the other in Low-Pass mode, may be connected in parallel, as shown in Fig. 2-11 to provide Band-Reject operation. Flat Amplitude response should be utilized in both channels.

The input signal should be connected to both inputs (IN 1 and IN 2). The outputs (OUT 1 and OUT 2) should be summed through 1 K, 1% resistors. The output signal is available at the common point of these resistors. This connection produces a passband insertion loss of 6 dB.

CAUTION

Both channels must be set to the same gain setting. If they are both set to 0 dB gain, the output will be 6 dB below the input level in the passband. If they are both set to 20 dB gain, the output will be 14 dB above the input level in the passband.

The rejection band in this configuration extends from the Low-Pass Cutoff Frequency to the High-Pass Cutoff Frequency. Again, the overall response may be determined by combining the normalized plots given in Figures 2-3 through 2-6.

f. Sharp-Notch Filter (Model 452 only)

The Sharp-Notch response shown in Fig. 2-12 is a special case of Band-Reject operation of Model 452. Input signal, channel connections, etc. should be made as described under Band-Reject filtering.

To obtain a notch (or null) at a desired frequency f_o , the High-Pass Cutoff Frequency is set to 1.75 f_o and the Low-Pass Cutoff Frequency is set to 0.57 f_o . For optimum rejection the High-Pass and Low-Pass settings should be alternatively adjusted, starting with the least significant digits.

CAUTION

While the maximum rejection obtainable in this mode of operation approaches the noise floor of the instrument, the maximum measurable rejection may be limited by the harmonic content of the input sinewave. In this mode of operation, it is thus possible to use the instrument for distortion analysis.

g. Low Pass or High Pass Filter with Doubled Rolloff

The two channels of the instrument may be cascaded as shown in Fig. 2-11. The Cutoff Frequencies of both channels are set to the same value and both channels are set to either High Pass, or Low Pass. Flat Amplitude response is utilized in both channels. Signal and channel connections are made as described under Band-Pass Filter and gain settings should also be made in accordance with the instructions given under Band-Pass Filter.

The overall response of this configuration may be determined by combining the normalized plots given in Figures 2–3 through 2–6. The Response at the Cutoff Frequency will now be 6 dB down and Rolloff will be 48 dB/octave for Model 452 and 96 dB/octave for Model 852.

2-7. OUTPUT SIGNAL

Full-scale output signal is specified as \pm 10 Volts and \pm 15 mA, max. Above 300 KHz, the output signal will follow the reduction in input signal shown in Fig. 2-2, provided the current required by the load connected to the instrument does not exceed the maximum value of \pm 15 mA. Heavy capacitive loads can easily exceed this current at high frequencies. For example, 25 feet of RG-58 cable is equivalent to a capacitance of 750 pf, which requires \pm 15 mA current at 300 KHz.

2-8. CUTOFF FREQUENCY OVERRANGE

The unmarked position between 0 and 10 on the Cutoff Frequency dials is an active position corresponding to the digit 11. If all Cutoff Frequency dials are set to this position a maximum setting of 122.1 (110 + 11 + 1.1) is available.

This position provides a 10% overrange relative to the specified maximum setting of 111.

2-9. MINIMUM CUTOFF FREQUENCY SETTING

The minimum valid setting of the Cutoff Frequency dials is 0.01. The setting 0.00 is not valid.

2-10 CUTOFF FREQUENCY RESOLUTION

The Cutoff Frequency dials should always be set for maximum resolution. For example, a cutoff frequency of 500 Hz may be set as 5.00×100 , 0.50×1 K, or 0.05×10 K. Of the above choices, 5.00×100 is the proper setting.

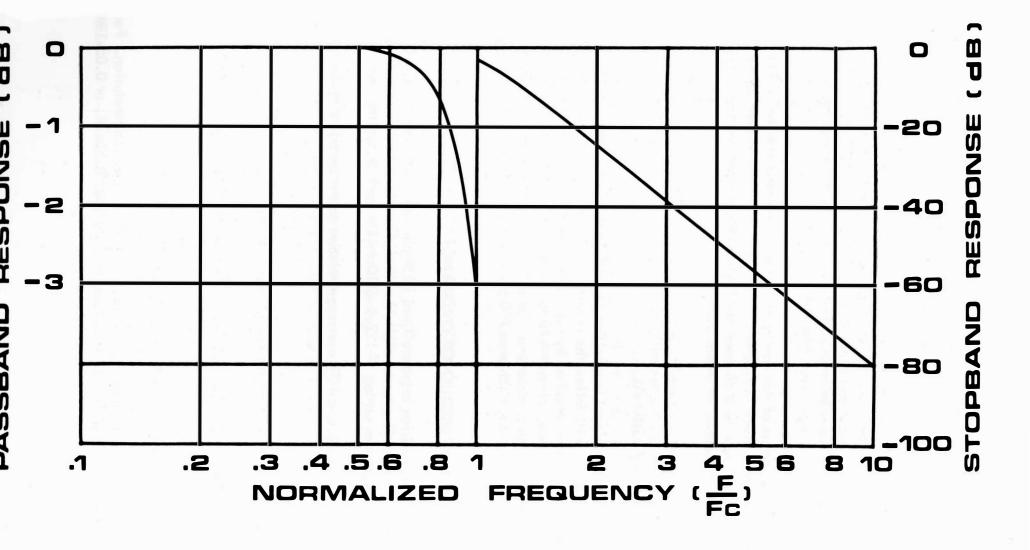


Fig. 2-3 452 Flat Ampl. Response - Lo Pass

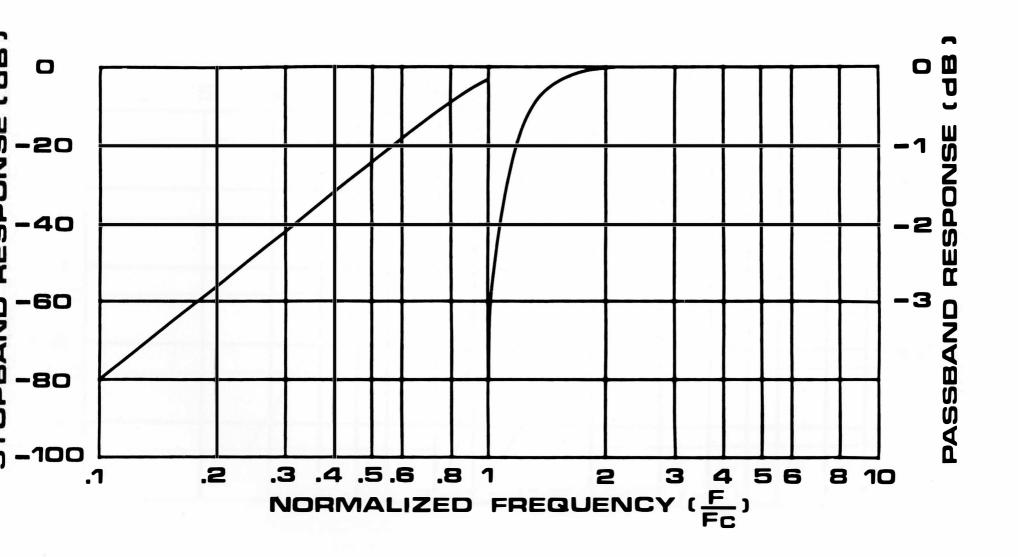
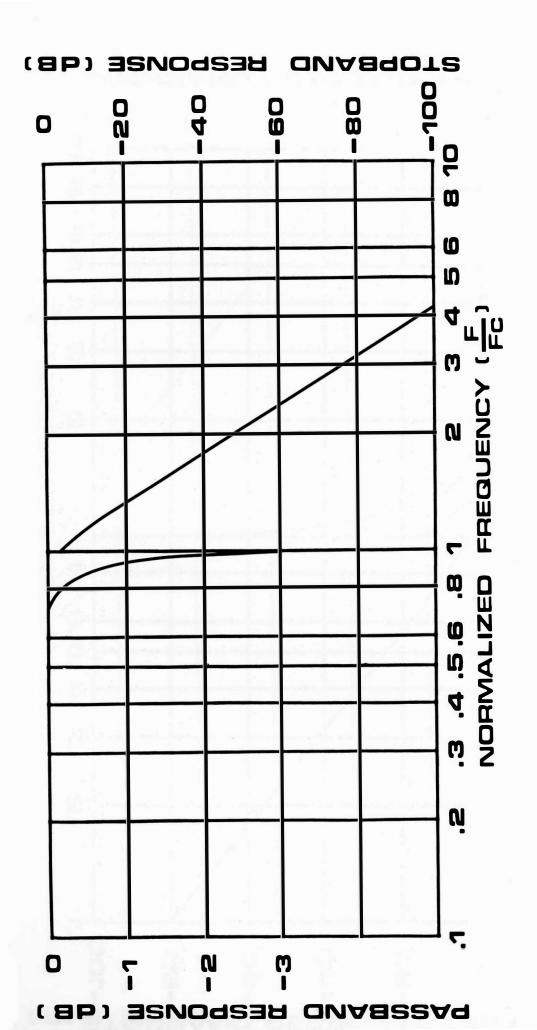


Fig. 2-4 452 Flat Ampl. Response - Hi Pass



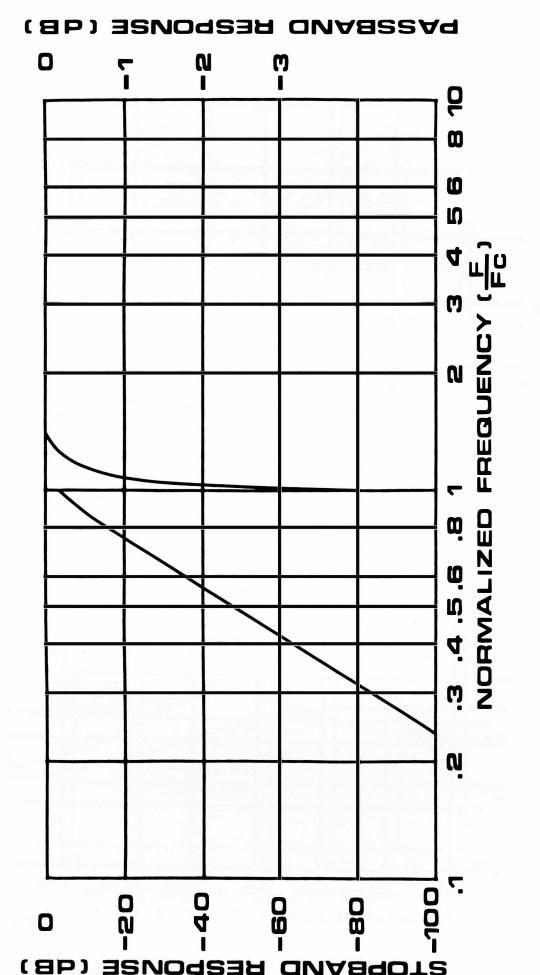


Fig. 2-6 852 Flat Ampl. Response - Hi Pass

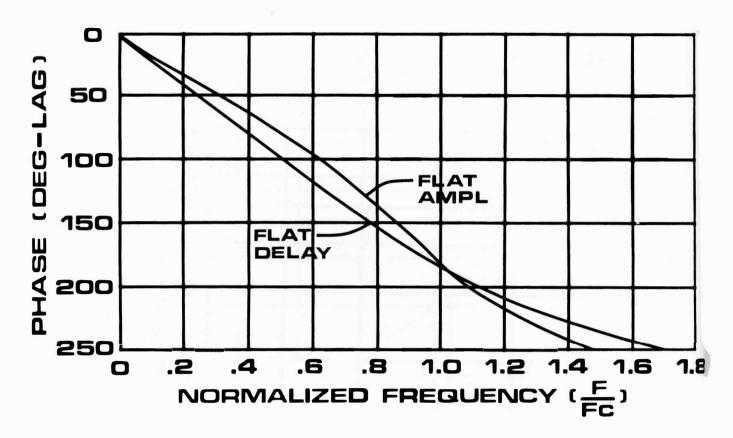


Fig. 2-7 452 Phase Response - Lo Pass

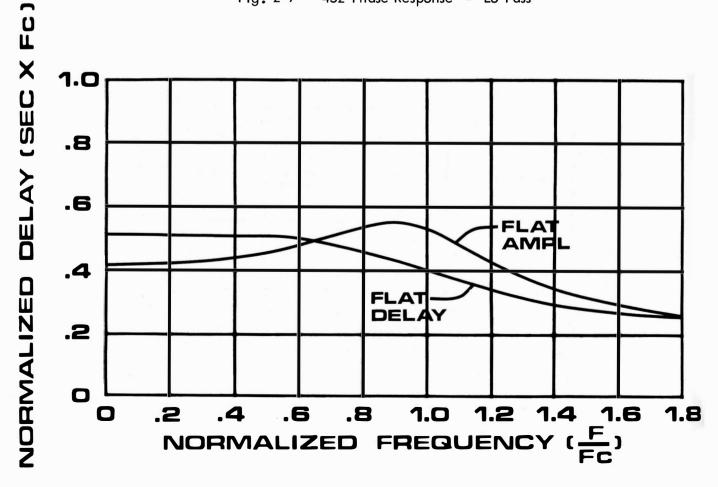


Fig. 2-8 452 Delay Response - Lo Pass

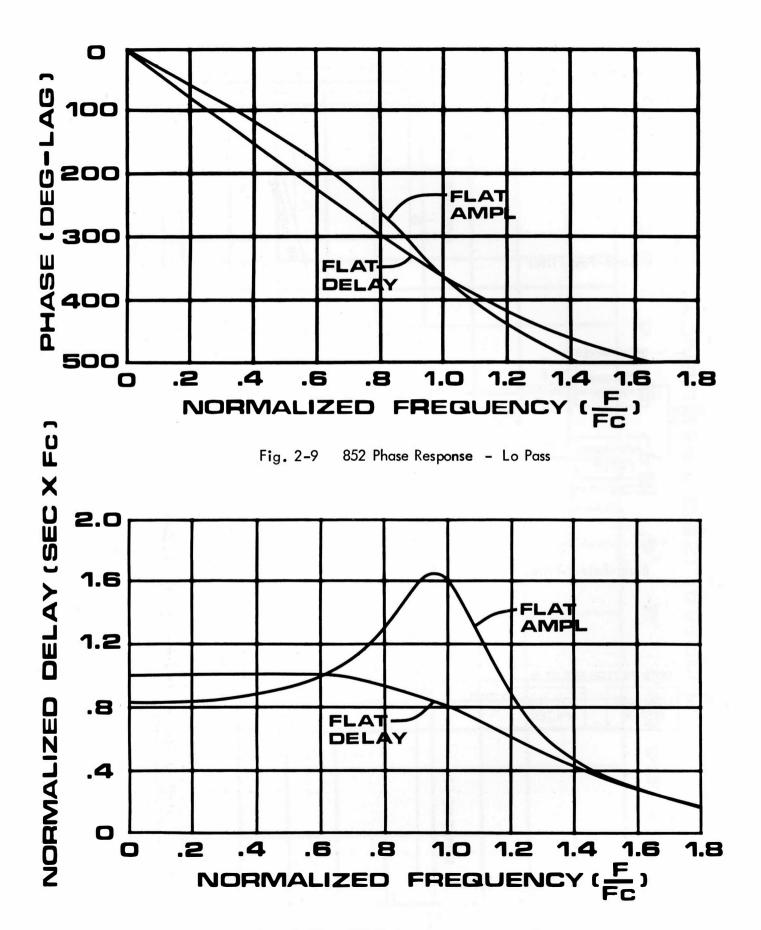
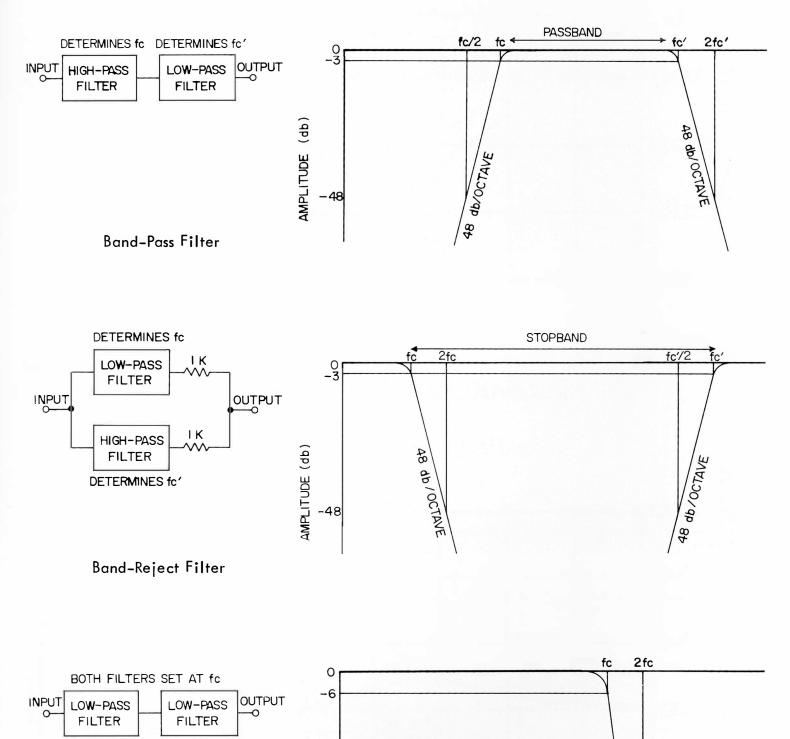


Fig. 2-10 852 Delay Response - Lo Pass



(qp) HAMPLITUDE (dp) AMPLITUDE (dp) Pass Filter with Doubled Rolloff

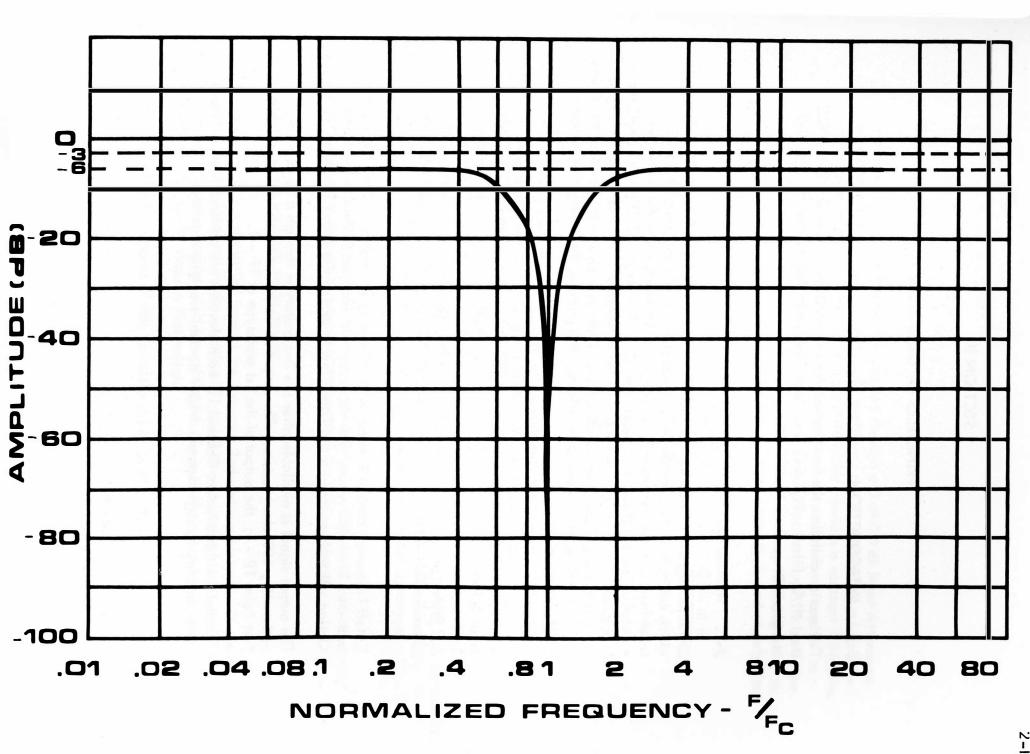


Fig. 2-12 452 Sharp Notch Response

SECTION III

PRINCIPLES OF OPERATION

3-1. INTRODUCTION

This section describes the basic principles of operation of Models 452 and 852 Dual Hi/Lo Filters. Fig. 3-1 is a Block Diagram of Model 452 and Fig. 3-2 is a Block Diagram of Model 852.

3-2. MODEL 452

The input signal of Channel 1 is applied through a 0 dB/20 dB Input Attenuator, which controls the two available gain positions, and is followed by a high input impedance buffer amplifier. The Input Attenuator provides a constant 1 Megohm input resistance in either position. The output of the Buffer amplifier is applied to a cascade of two "2nd-Order Prototypes". A "2nd-Order Prototype" is an active RC, 2nd-order (12 dB/octave) filter section which is used as a building block to synthesize higher-order filters. The gains of these stages at dc and at cutoff are as follows:

	Gain at dc	Gain at fc
Input Attenuator	0.0 dB / - 20.0 dB	$0.0 \overline{dB/-20.0} dB$
Input Buffer	+11.8 dB	+11.8 dB
1st Prototype	+ 1.2 dB	- 4.1 dB
2nd Prototype	+ 7.0 dB	+ 9.3 dB
Overall (OUT/IN)	+20.0 dB/0.0 dB	+17.0 dB/ - 3.0 dB

Cutoff Frequency control is obtained by changing the resistors of the filter stages in 8 - 4 - 2 - 1 BCD steps. The capacitors are changed in decade steps and Option -01 adds an extra set of capacitors to extend the cutoff frequency coverage.

The output signal is available after the 2nd prototype through a 50-ohm (or, optionally, 600-ohm) resistor. The output of the buffer amplifier is available at Test Point TP - 1; the output of the 1st prototype at TP - 2.

Channel 2 is identical to Channel 1. Both channels are powered from one main power supply, through separate $\pm 15 \,\mathrm{V}$ dc dual-tracking regulators.

3-3. MODEL 852

The input signal of Channel 1 is applied through a 0 dB/20 dB Input Attenuator, which controls the two available gain positions, and is followed by a high input impedance buffer amplifier. The Input Attenuator provides a constant 1 Megohm resistance in either position. The output of the Buffer amplifier is applied to a cascade of four "2nd-Order Prototypes". A "2nd-Order Prototype" is an active RC, 2nd-order (12 dB/octave) filter section which is used as a building block to synthesize higher-order filters. The gains of these stages at dc and at cutoff are as follows:

	Gain at dc	Gain at fc
Input Attenuator	0.0 dB / - 20.0 dB	0.0 dB / - 20.0 dB
Input Buffer	+3.4 dB	+3.4 dB
1st Prototype	+0.3 dB	-5.5 dB
2nd Prototype	+2.5 dB	-1.9 dB
3rd Prototype	+5.5 dB	+4.6 dB
4th Prototype	+8.3 dB	+16.5 dB
Overall (OUT/IN)	+20.0 dB/0.0 dB	+17.0 dB / -3.0 dB

Cutoff Frequency control is obtained by changing the resistors of the filter in 8 - 4 - 2 - 1 BCD steps. The capacitors are changed in decade steps and Option -01 adds an extra set of capacitors to extend the cutoff frequency coverage.

The output signal is available after the 4th prototype through a 50-ohm (or, optionally, 600-ohm) resistor. The output of the buffer amplifier is available at Test Point TP - 1; the output of the 1st prototype at TP - 2; the output of the 2nd prototype at TP - 3; and the output of the 3rd prototype at TP -4.

Channel 2 is identical to Channel 1. Both channels are powered from one main power supply, through separate \pm 15 V dc dual-tracking regulators.

3-4. 2nd - ORDER PROTOTYPE

Figure 3–3 is a simplified from of the low-pass 2nd-order prototype. The high-pass prototype is identical to the circuit of Figure 3–3 except that the position of resistors R and capacitors C is interchanged. In both Models the interchange is effected by the Hi Pass/Lo Pass switch.

The amplitude response of this circuit is shown in Fig. 3-4.

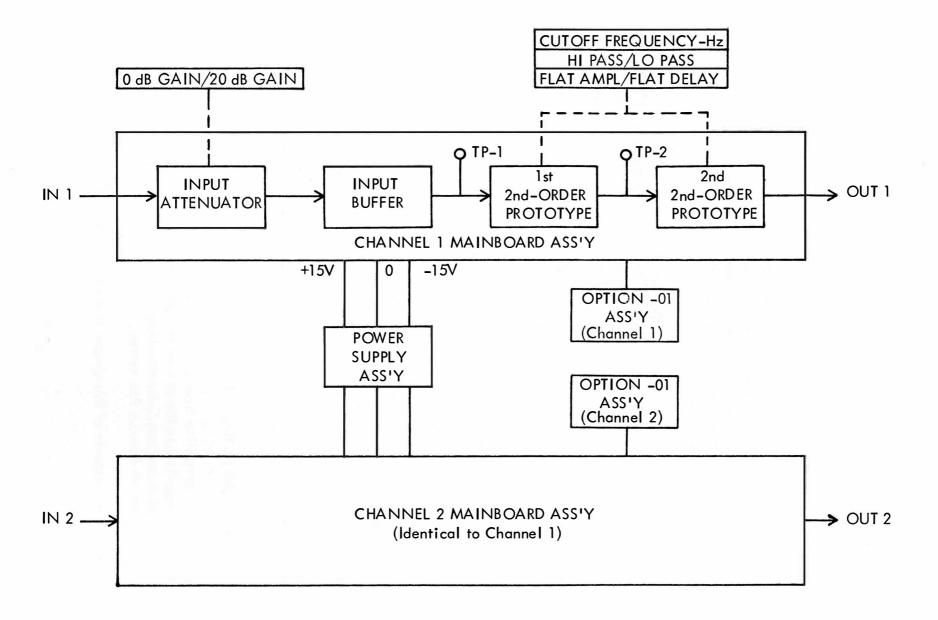


Fig. 3-1. Model 452 Block Diagram

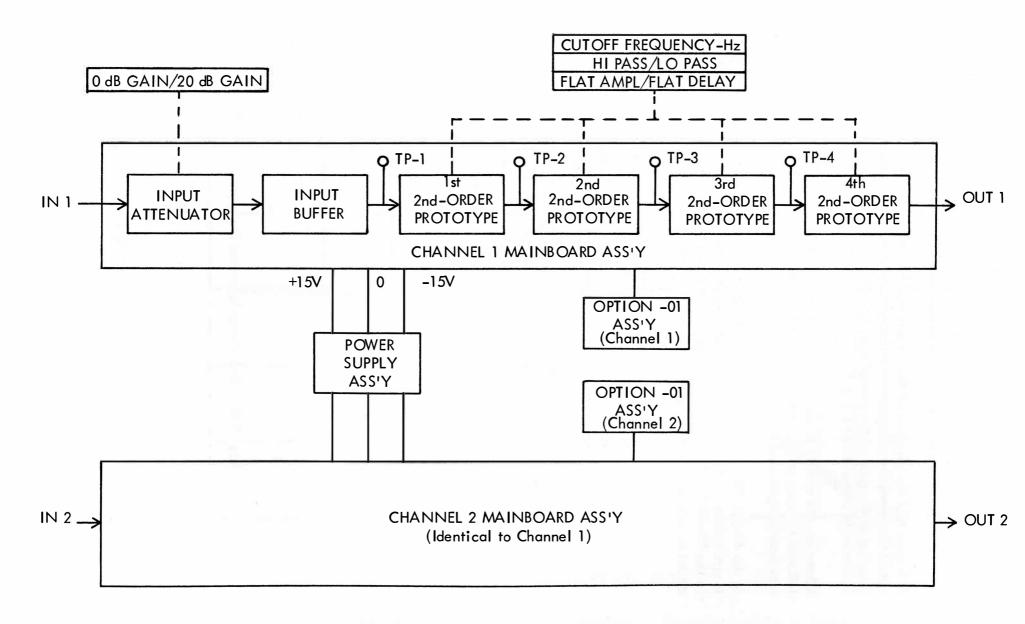


Fig. 3-2. Model 852 Block Diagram

It is seen that the response of the circuit may be altered in the vicinity of the cutoff frequency by changing the value of damping β . The damping is a function of the gain of the operational amplifier which, in turn, is determined by the ratio of resistors R1 and R2.

Likewise, the overall response of a cascade of such prototype sections may be tailored by appropriate selection of damping and the desired higher-order filter may thus be synthesized.

In the Model 452, a fourth order Flat-Amplitude, or Butterworth filter (per channel) is synthesized in this manner, while an eighth-order Butterworth filter is synthesized in the Model 852. The Flat-Delay or Linear Phase response is obtained in either model by appropriate changes in the damping of the prototype sections.

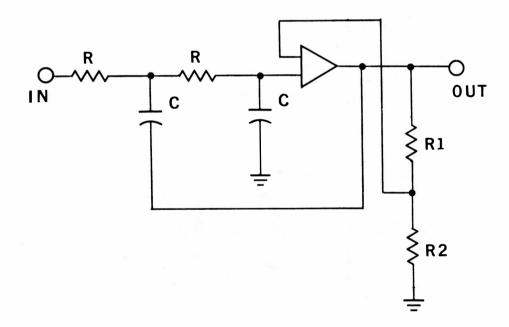


Fig. 3-3. 2nd Order Low-Pass Prototype

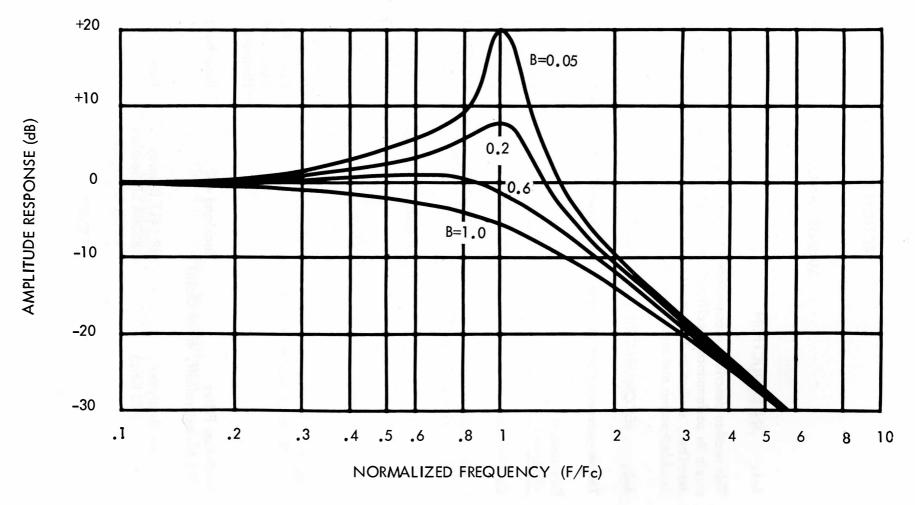


Fig. 3-4. Response of 2nd order Low-Pass Prototype for various values of damping B

SECTION IV

MAINTENANCE

4-1. INTRODUCTION

This section describes recommended test procedures to verify that the instrument meets its performance specifications. In addition, adjustment procedures are described, so that an instrument may be calibrated to meet its specifications. Troubleshooting and repair procedures are also included.

4-2. RECOMMENDED TEST EQUIPMENT

The recommended test equipment and its use is listed below:

Description		
(Feature)	Model	Tests
Oscilloscope	Tektronix 475	Waveform viewing
Digital Multimeter (100 uV dc resolution)	Keithley 168	DC Offset
AC Voltmeter (1% accuracy)	HP 400FL	Passband Gain, Cutoff Frequency Accuracy
RMS Voltmeter (True RMS)	Ballantine 3620A	Broadband Noise
Frequency Synthesizer (> -70 dB harmonics at 1 KHz)	Rockland 5100	Passband Gain, Cutoff Frequency Accuracy, Max. Stopband Attenuation, Harmonic Components
Band-Pass Filter (24 dB/oct rolloff, 40 dB Gain)	Rockland 452	Broadband Noise
Spectrum Analyzer (20 Hz – 300 KHz)	HP 141T Display 8556A LF Section 8552B IF Section	Max. Stopband Attenuation
Spectrum Analyzer (5 Hz – 50 KHz)	HP 3580A	Harmonic Components, AC Line-related Spurious

Description (Feature)	Model	Tests
Gain/Phase Meter (1 Hz – 13 MHz)	HP 3575A	Adjustments
50 - ohm Termination	-	2 - HT15
5 K load resistor	-	= -
1 KHz Notch Filter	Assemble as shown below	Harmonic Components

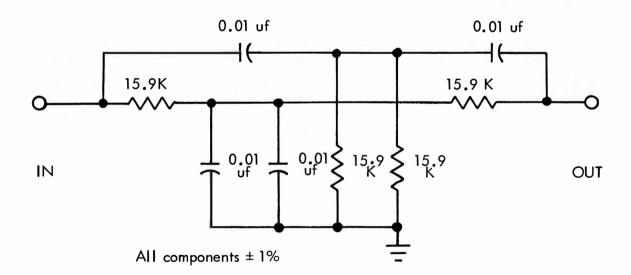
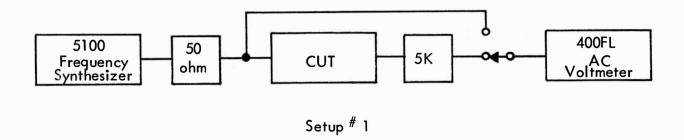
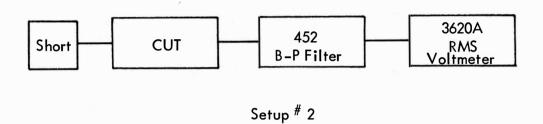


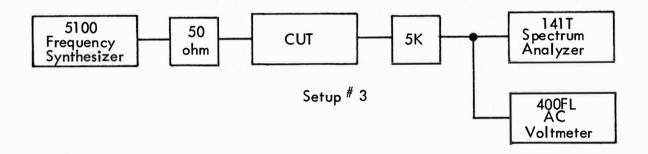
Fig. 4-1. 1 KHz Notch Filter

WARNING

The specifications of these instruments cannot be verified, unless the recommended equipment (or equal) is utilized in test. In particular, Function Generators cannot be used in place of the recommended signal source. Function Generators produce high harmonics in their output waveform and will cause considerable errors in certain tests requiring the use of a signal source.







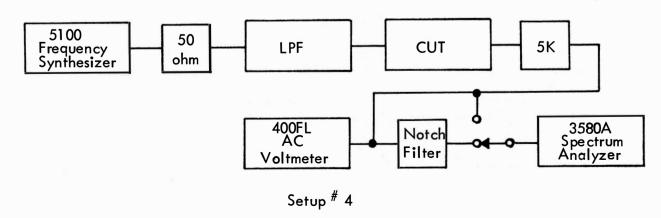


Fig. 4.2. Performance Test Setups

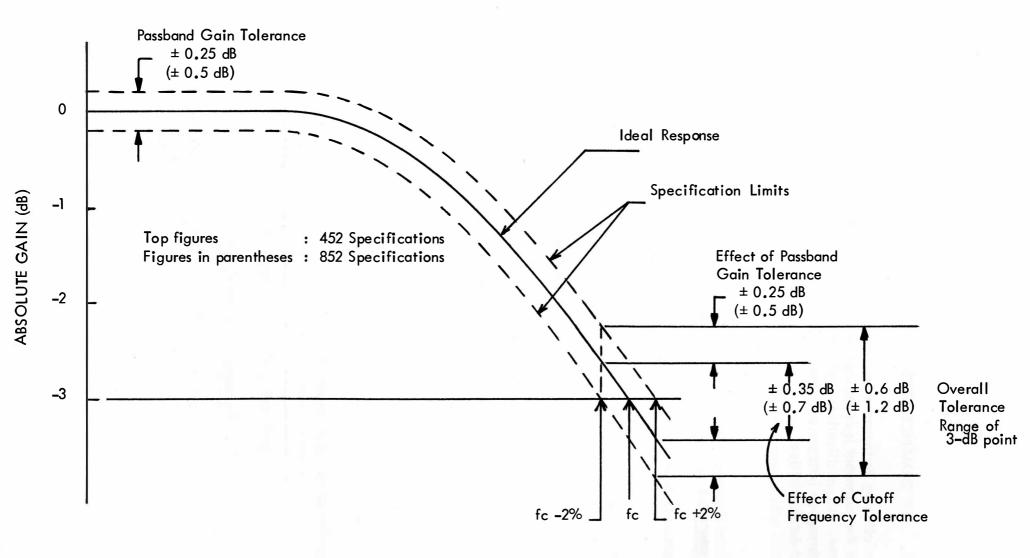


Fig. 4-3. Passband Gain & Cutoff Frequency Tolerances

4-3. PERFORMANCE TESTS

The following Performance Tests are procedures which can be used to verify that the instrument is operating properly and meets the specifications listed below. All specifications apply to Butterworth (Flat Ampl.) response and all Performance Tests are performed with the Flat Ampl./Flat Delay switch in the Flat Ampl. position.

Specification

Parameter	<u>Model 452</u>	Model 852		
Passband Gain Accuracy	0 ±0.25 dB, 20 ±0.25 dB (±0.5 dB, HP,×10K)	0 ±0.5 dB, 20 ±0.5 dB (±1dB,HP,×10K)		
Cutoff Frequency Calibration Accuracy	±2%	±2%		
DC Offset	$0\pm0.5~\text{mV}~\text{dc}$	$0\pm2.5~\text{mV}~\text{dc}$		
Broadband Noise	100 uV rms, max.	200 υV rms, max.		
Maximum Stopband Attenuation*	90 dB	90 dB		
Harmonic Components*	-90 dB	-80 dB		
AC Line-related Spurious Components*	-110 dB	-100 dB		
* relative to full-scale signal of 7.1 V rms (+17 dBV)				

a. Passband Gain Accuracy (See Fig. 4-3)

Connect equipment as shown in Setup #1. Set Frequency Synthesizer output to 0.71 V rms and measure passband gain of the Channel Under Test (CUT) for the settings shown in Table 4.1.

b. Cutoff Frequency Calibration Accuracy (See Fig. 4-3)

With the equipment connected as shown in Setup #1, set CUT gain to 0 dB and the Frequency Synthesizer output to 0.0 dBV. At each Cutoff Frequency setting shown in Table 4.2 set the Synthesizer frequency equal to the Cutoff Frequency setting.

The \pm 2% specification on Cutoff Frequency Calibration Accuracy is met if the output level falls within the tolerance limits shown in Fig. 4-3, namely:

Model 452 : $-3dBV \pm 0.6dB$

 $(-3dBV \pm 0.85dB, in \times 10K, HP)$

Model 852 : $-3dBV \pm 1.2dB$

 $(-3dBV \pm 1.7dB, in \times 10K, HP)$

c. DC Offset

Connect a short across the input connector of the Channel Under Test (CUT) and the DC Multimeter across the output connector. Allow at least 10 minutes for the instrument to warm up under its own power and measure the DC Offset for the settings shown in Table 4.3.

d. <u>Broadband Noise</u>

Connect equipment as shown in Setup #2. Connect a short across the input connector of the Channel Under Test and set the Ground/Float switch on the rear panel to the Float position. Turn off all unused equipment in the vicinity of the test area and disconnect it from the instrument under test.

Connect the 452 Post Filter/Amplifier as a Band-Pass filter with the following settings:

CH 1: 0.01 x 10 Cutoff Frequency

Hi Pass

20 dB Gain Flat Ampl.

CH 2: 10.00 x 10K Cutoff Frequency

Lo Pass 20 dB Gain Flat Ampl. With the above settings, the 452 Post Filter/Amplifier provides 40 dB of gain and establishes a noise measurement bandwidth of 0.1 Hz to 100 KHz. (A noise bandwidth of 100 KHz is, for all practical purposes, equal to the 3-dB bandwidth of a 4th-order filter.)

Measure noise with the 3620A RMS Voltmeter for the CUT settings shown in Table 4.4. Output Broadband Noise of the CUT is calculated as follows:

Output Noise =
$$\frac{1}{100}$$
 x Voltmeter Reading

e. Maximum Stopband Attenuation

Connect equipment as shown in Setup # 3 and set the Channel Under Test as follows:

1.00 x 10 K Cutoff Frequency Hi Pass 20 dB Gain Flat Ampl.

Set the 5100 Frequency Synthesizer to 100 KHz and increase its output amplitude until CUT output is equal to full-scale signal of 7.1 V rms (\pm 17 dBV).

Set the 141T Spectrum Analyzer controls as follows:

Input Level : -10 dBV
Bandwidth : 300 Hz
Scan Width : 2 KHz/div
Scan Time : 50 msec

Log Ref Level: Adjust for full-scale Display after tuning analyzer

to 100 KHz

Set the CUT and input frequency to the values shown in Table 4.5. In each case, tune the Spectrum Analyzer to the input frequency and increase Input Level control setting to -60 dBV. Read the amplitude of the signal displayed on the screen. The Maximum Stopband Attenuation with respect to full-scale signal is calculated as follows:

$$A = (50 dB + Display dB)$$

f. Harmonic Components

Because of the extremely low distortion of these instruments, a special measurement procedure must be employed. The arrangement shown in Setup # 4 is recommended. Here, the unused channel of the instrument is employed as a Low-Pass Filter to reduce the harmonic components of the 5100 Frequency Synthesizer to levels of -100 dB or less. The output of the Channel Under Test (CUT) is viewed on the 3580 A Spectrum Analyzer directly, or through a passive Notch Filter centered on the measurement frequency. For the values shown, the Notch Filter will attenuate the fundamental (1 KHz) by at least 50 dB, while the 2nd harmonic is attenuated 10 dB and the 3rd harmonic 6 dB.

Set the Synthesizer frequency to 1.000 KHz and the Low Pass Filter to a Cutoff Frequency of 1.00 \times 1 K, 0 dB Gain, Flat Ampl. response. Set the Channel Under Test as follows:

```
1.00 x 10 Cutoff Frequency
Hi Pass
20 dB Gain
Flat Ampl.
```

Increase Synthesizer amplitude until full-scale signal of 7.1 V rms (\pm 17 dBV) appears at the output of the CUT.

Connect the 3580 A Spectrum Analyzer to the output of the CUT and set its controls as follows:

Bandwidth : 30 Hz
Freq. Span : .5 KHz/div
Sweep Time : 1 sec/div
Display : LOG, 10 dB
Input Sensitivity : +10 dBV

Input Sensitivity Vernier: Adjust to obtain full-scale (0 dB) Display

at 1 KHz.

Amplitude Ref Level : Normal

Connect the Spectrum Analyzer to the output of the Notch Filter and increase Input Sensitivity to -30 dBV. Read the amplitude of each harmonic component displayed on the screen. Harmonic Components at the output of the CUT with respect to full-scale signal are calculated as follows:

```
2nd Harmonic = -(40 dB + 2nd Harm. Display dB) + 10 dB
3rd Harmonic = -(40 dB + 3rd Harm. Display dB) + 6 dB
4th Harmonic = -(40 dB + 4th Harm. Display dB) + 4 dB
```

g. A-C Line-related Spurious Components

Connect a short across the input connector of the Channel Under Test and the 3580A Spectrum Analyzer to the output connector. Set the Ground/Float switch on the rear panel to the Float position and turn off all other equipment in the vicinity of the test area. Disconnect all other equipment from the instrument under test.

Set the Channel Under Test as follows:

10.00 x 10 K Cutoff Frequency Lo Pass 0 dB Gain Flat Ampl.

Set the 3580A Spectrum Analyzer controls as follows:

Input Sensitivity : -30 dBV
Input Sensitivity Vernier : CAL
Bandwidth : 3 Hz
Freq. Span : 20 Hz/div
Sweep Time: : 5 sec/div
Display : LOG, 10 dB

Amplitude Ref Level : Normal

Obtain a complete sweep on the analyzer screen and measure the amplitude of the Display at line frequency and multiples ($\times 2$, $\times 3$) of the line frequency. Line-related spurious components at the output of the CUT with respect to full-scale signal (+ 17 dBV) are calculated as follows:

Spurious = -(47 dB + Display dB)

PERFORMANCE TEST RESULTS

Rockland Model 452	Option-	Test By
Dual Hi/Lo Filter		Date
Serial Number		
Channel 1 2		

Table 4.1. Passband Gain Accuracy

Cutoff			Input	Passbo	and Gain
Frequency	Mode	Gain	Frequency	Specification	Measured
10.00 x 1K	LP	0 dB	1 KHz	0 ± .25 dB	21 00 E
$10.00 \times 1K$	LP	20 dB	1 KHz	$20 \pm .25 dB$	
$1.00 \times 1K$	HP	0 dB	10 KHz	0 ± .25 dB	The state of the s
$1.00 \times 1K$	HP	20 dB	10 KHz	$20 \pm .25 dB$	
$1.00 \times 10K$	HP	0 dB	100 KHz	$0 \pm .5 dB$	
$1.00 \times 10K$	HP	20 dB	100 KHz	$20 \pm .5 dB$	

Table 4.2. Cutoff Frequency Calibration Accuracy

Cutoff Frequency	Mode	Input Frequency	Output level Specification Limits	Measured
$10.00 \times 10K$	LP	100.0 KHz	-2.40 dBV to -3.60 dBV	
$10.00 \times 10K$	HP	100.0 KHz	-2.15 dBV to -3.85 dBV	
$1.00 \times 10K$	LP	10.0 KHz	-2.40 dBV to -3.60 dBV	The state of the s
$1.00 \times 10K$	HP	10.0 KHz	-2.15 dBV to -3.85 dBV	734 734 734 734 734 734 734 734 734 734
$10.00 \times 1K$	LP	10.0 KHz	-2.40 dBV to -3.60 dBV	
$10.00 \times 1K$	HP	10.0 KHz	-2.40 dBV to -3.60 dBV	33 22 23 30 30 30
10.00×100	LP	1.0 KHz	-2.40 dBV to -3.60 dBV	72 77 77
10.00×100	HP	1.0 KHz	-2.40 dBV to -3.60 dBV	
10.00×10	LP	100 Hz	-2.40 dBV to -3.60 dBV	
10.00×10	HP	100 Hz	-2.40 dBV to -3.60 dBV	
Option-01:				
10.00 x 1	LP	10 Hz	-2.40 dBV to -3.60 dBV	1

-2.40 dBV to -3.60 dBV

 10.00×1

ΗP

10 Hz

Table 4.2. Cutoff Frequency Calibration Accuracy - continued

Cutoff Frequency	Mode	Input Frequency	Output level Specification limits	Measured
10.00 x 1K	LP	10.00 KHz	-2.40 dBV to -3.60 dBV	1 " "
9.00 x 1K	LP	9.00 KHz	-2.40 dBV to -3.60 dBV	
8.00 x 1K	LP	8.00 KHz	-2.40 dBV to -3.60 dBV	
7.00 x 1K	LP	7.00 KHz	-2.40 dBV to -3.60 dBV	
6.00 x 1K	LP	6.00 KHz	-2.40 dBV to -3.60 dBV	
$5.00 \times 1K$	LP	5.00 KHz	-2.40 dBV to -3.60 dBV	
4.00 x 1K	LP	4.00 KHz	-2.40 dBV to -3.60 dBV	
$3.00 \times 1K$	LP	3.00 KHz	-2.40 dBV to -3.60 dBV	
2.00 x 1K	LP	2.00 KHz	-2.40 dBV to -3.60 dBV	
1.00 x 1K	LP	1.00 KHz	-2.40 dBV to -3.60 dBV	
$1.00 \times 1K*$	LP	1.00 KHz	-2.40 dBV to -3.60 dBV	
$0.90 \times 1K$	LP	900 Hz	-2.40 dBV to -3.60 dBV	
$0.80 \times 1K$	LP	800 Hz	-2.40 dBV to -3.60 dBV	
$0.70 \times 1K$	LP	700 Hz	-2.40 dBV to -3.60 dBV	
$0.60 \times 1K$	LP	600 Hz	-2.40 dBV to -3.60 dBV -	
$0.50 \times 1K$	LP	500 Hz	-2.40 dBV to -3.60 dBV -	
$0.40 \times 1K$	LP	400 Hz	-2.40 dBV to -3.60 dBV -	
$0.30 \times 1K$	LP	300 Hz	-2.40 dBV to -3.60 dBV	
$0.20 \times 1K$	LP	200 Hz	-2.40 dBV to -3.60 dBV	
$0.10 \times 1K$	LP	100 Hz	-2.40 dBV to -3.60 dBV	
$0.10 \times 1K^*$	LP	100 Hz	-2.40 dBV to -3.60 dBV	
$0.09 \times 1K$	LP	90 Hz	-2.40 dBV to -3.60 dBV	
$0.08 \times 1K$	LP	80 Hz	-2.40 dBV to -3.60 dBV	
$0.07 \times 1K$	LP	70 Hz	-2.40 dBV to -3.60 dBV	
$0.06 \times 1K$	LP	60 H z	-2.40 dBV to -3.60 dBV	
$0.05 \times 1K$	LP	50 Hz	-2.40 dBV to -3.60 dBV	
$0.04 \times 1K$	LP	40 Hz	-2.40 dBV to -3.60 dBV	
$0.03 \times 1K$	LP	30 Hz	-2.40 dBV to -3.60 dBV	
$0.02 \times 1K$	LP	20 Hz	-2.40 dBV to -3.60 dBV	7.1
$0.01 \times 1K$	LP	10 Hz	-2.40 dBV to -3.60 dBV	
			-	

^{*} Use the "10" of the next lower digit to obtain this setting.

Table 4.3. D.C. Offset

Cutoff Frequency	Mode	Gain	Specification	Measured
10.00 x 10K	LP	0 dB	± 0.5 mV dc	28 February Braddook
$10.00 \times 10K$	LP	20 dB	± 0.5 mV dc	
0.01×10	HP	0 dB	± 0.5 mV dc	
0.01×10	HP	20 dB	\pm 0.5 mV dc	

Table 4.4. Broadband Noise

Cutoff <u>Frequency</u>	Mode	Gain	Specification	Measured
10.00 x 10K	LP	0 dB	100 uV rms, max	
$10.00 \times 10K$	LP	20 dB	100 uV rms, max	
0.01×10	HP	0 dB	100 uV rms, max	
0.01×10	HP	20 dB	100 υV rms, max	

Table 4.5. Maximum Stopband Attenuation

Cutoff Frequency	Mode	Input Frequency	Specification	Measured
1.00 x 10K	LP	200 KHz	90 dB	
10.00 x 10K	HP	5 KHz	90 dB	

Table 4.6. Harmonic Components

	Specification	Measured
2nd Harmonic	-90 dB	-5.1
3rd Harmonic	- 90 dB	
4th Harmonic	-90 dB	

Table 4.7. Line-Related Spurious Components

	Specification	Measured
Line Frequency 2 x Line Frequency 3 x Line Frequency	-110 dB -110 dB -110 dB	

PERFORMANCE TEST RESULTS

Rockland Model 852	Option-		Test By	
Dual Hi/Lo Filter			Date	
Serial Number				
Channel 1	2			
	Table 4.1.	Passband Gain	Accuracy	
Cutoff		Input	Passband Gain	

Cutoff			Input	Pas	ssband Gain
Frequency	Mode	Gain	Frequency	<u>Specification</u>	Measured
10.00 x 1K	LP	0 dB	1 KHz	$0 \pm .5 dB$	
$10.00 \times 1K$	LP	20 dB	1 KHz	$20 \pm .5 dB$	
$1.00 \times 1K$	HP	0 dB	10 KHz	$0 \pm .5 dB$	
$1.00 \times 1K$	HP	20 dB	10 KHz	$20 \pm .5 dB$	
$1.00 \times 10K$	HP	0 dB	100 KHz	$0 \pm 1 dB$	5 × 00 × 1 × 0 × 0 × 0 × 0 × 0 × 0 × 0 ×
1.00 x 10K	HP	20 dB	100 KHz	$20 \pm 1 dB$	

Table 4.2. Cutoff Frequency Calibration Accuracy

Cutoff		Input	Output level	
Frequency	Mode	Frequency	Specification Limits	Measured
10.00 x 10K	LP	100.0 KHz	-1.8 dBV to -4.2 dBV	
$10.00 \times 10K$	HP	100.0 KHz	-1.3 dBV to -4.7 dBV	
$1.00 \times 10K$	LP	10.0 KHz	-1.8 dBV to -4.2 dBV	
$1.00 \times 10K$	HP	10.0 KHz	-1.3 dBV to -4.7 dBV	
$10.00 \times 1K$	LP	10.0 KHz	-1.8 dBV to -4.2 dBV	
$10.00 \times 1K$	HP	10.0 KHz	-1.8 dBV to -4.2 dBV	
10.00×100	LP	1.0 KHz	-1.8 dBV to -4.2 dBV	
10.00×100	HP	1.0 KHz	-1.8 dBV to -4.2 dBV	
10.00×10	LP	100 Hz	-1.8 dBV to -4.2 dBV	
10.00×10	HP	100 Hz	-1.8 dBV to -4.2 dBV	
Option -01:				
10.00 x 1	LP	10 Hz	-1.8 dBV to -4.2 dBV	

10 Hz

 10.00×1

HP

-1.8 dBV to -4.2 dBV

Table 4.2. Cutoff Frequency Calibration Accuracy - continued

Cutoff Frequency	Mode	Input Frequency	Output level Specification Limits		Med	asured
10.00 x 1K	LP	10.00 KHz	-1.8 dBV to -4.2 dBV		1	
$9.00 \times 1K$	LP	9.00 KHz	-1.8 dBV to -4.2 dBV			
$8.00 \times 1K$	LP	8.00 KHz	-1.8 dBV to -4.2 dBV			
$7.00 \times 1K$	LP	7.00 KHz	-1.8 dBV to -4.2 dBV			
$6.00 \times 1K$	LP	6.00 KHz	-1.8 dBV to -4.2 dBV		9.0	4.4
$5.00 \times 1K$	LP	5.00 KHz	-1.8 dBV to -4.2 dBV			
$4.00 \times 1K$	LP	4.00 KHz	-1.8 dBV to -4.2 dBV		1	
$3.00 \times 1K$	LP	3.00 KHz	-1.8 dBV to -4.2 dBV			
$2.00 \times 1K$	LP	2.00 KHz	-1.8 dBV to -4.2 dBV			A 00 3 5 1
$1.00 \times 1K$	LP	1.00 KHz	-1.8 dBV to -4.2 dBV			8 99,00
$1.00 \times 1K*$	LP	1.00 KHz	-1.8 dBV to -4.2 dBV			N. 19 S.W.
$0.90 \times 1K$	LP	900 Hz	-1.8 dBV to -4.2 dBV	-A.F. T.	187.4	
$0.80 \times 1K$	LP	800 Hz	-1.8 dBV to -4.2 dBV	V 1/2		
$0.70 \times 1K$	LP	700 Hz	-1.8 dBV to -4.2 dBV			
$0.60 \times 1K$	LP	600 Hz	-1.8 dBV to -4.2 dBV		1.00	
$0.50 \times 1K$	LP	500 Hz	-1.8 dBV to -4.2 dBV			
$0.40 \times 1K$	LP	400 Hz	-1.8 dBV to -4.2 dBV			
$0.30 \times 1K$	LP	300 Hz	-1.8 dBV to -4.2 dBV			COCHALEST E A
$0.20 \times 1K$	LP	200 Hz	-1.8 dBV to -4.2 dBV			
$0.10 \times 1K$	LP	100 Hz	-1.8 dBV to -4.2 dBV		27.01	7. 904.5
$0.10 \times 1K*$	LP	100 Hz	-1.8 dBV to -4.2 dBV		77.7	7 A 87 A 11 A
$0.09 \times 1K$	LP	90 Hz	-1.8 dBV to -4.2 dBV			
$0.08 \times 1K$	LP	80 Hz	-1.8 dBV to -4.2 dBV			
$0.07 \times 1K$	LP	70 Hz	-1.8 dBV to -4.2 dBV			
$0.06 \times 1K$	LP	60 Hz	-1.8 dBV to -4.2 dBV	4-25-12-12-12-12-12-12-12-12-12-12-12-12-12-		
$0.05 \times 1K$	LP	50 Hz	-1.8 dBV to -4.2 dBV			
$0.04 \times 1K$	LP	40 Hz	-1.8 dBV to -4.2 dBV			
$0.03 \times 1K$	LP	30 Hz	-1.8 dBV to -4.2 dBV	1 1971		
$0.02 \times 1K$	LP	20 Hz	-1.8 dBV to -4.2 dBV		V 91.94	
$0.01 \times 1K$	LP	10 Hz	-1.8 dBV to -4.2 dBV		F-15/60	

^{*} Use the "10" of the next lower digit to obtain this setting.

Table 4.3. D.C. Offset

Cutoff Frequency	Mode	Gain	Specification	Measured
10.00 × 10K	LP	0 dB	± 2.5 mV dc	
$10.00 \times 10K$	LP	20 dB	± 2.5 mV dc	
0.01×10	HP	0 dB	$\pm 2.5 \text{ mV dc}$	
0.01×10	HP _	20 dB	\pm 2.5 mV dc	

Table 4.4. Broadband Noise

Cutoff Frequency	Mode	Gain	Specification	Measured
10.00 x 10K	LP	0 dB	200 uV rms, max	
$10.00 \times 10K$	LP	20 dB	200 uV rms, max	
0.01×10	HP	0 dB	200 uV rms, max	
0.01×10	HP	20 dB	200 uV rms, max	

Table 4.5. Maximum Stopband Attenuation

Cutoff Frequency	Mode	Input Frequency	Specification	Measured
1.00 x 10K	LP	200 KH z	90 dB	
10.00 x 10K	HP	5 KH z	90 dB	

Table 4.6. Harmonic Components

	<u>Specification</u>	Measured
2nd Harmonic 3rd Harmonic 4th Harmonic	-80 dB -80 dB -80 dB	

Table 4.7. Line-Related Spurious Components

	<u>Specification</u>	Measured
Line Frequency 2 x Line Frequency 3 x Line Frequency	-100 dB -100 dB -100 dB	

4-4. ADJUSTMENTS*

a. DC Offset Adjustment

This adjustment may be performed if the output dc level is determined to be out of specification. The adjustment should be performed after allowing at least 10 minutes for the instrument to warm up under power. Connect a short across the input connector of the instrument and the DC Multimeter across the output connector. Perform the adjustments shown below:

Cutoff Freq.	Mode	Gain	Response	Adjustment and 452: Vo	Output V 852 : Vo
10.00 x 1K	Hi Pass	20 dB	•	R23 : ±0.5 mV	R27: ± 2.5 mV
0.01 x 1K	Lo Pass	20 dB		R8 : ±0.5 mV	R8: ± 2.5 mV

b. Attenuator Response Adjustment

This adjustment may be performed if the response at 100 KHz in high-pass mode and 0 dB gain is out of specification. Connect the Frequency Synthesizer to the input of the instrument and the Gain/Phase Meter betwen input and output. Use the following settings:

Input Frequency: 100 KHz / 1 KHz
Amplitude: 1.0 V rms
Filter Settings: 5.00 x 10
Hi Pass
0 dB Gain
Flat Ampl.

Model 452: Adjust C1 to obtain same gain at 100 KHz as at 1 KHz (within ± 0.25 dB)

Model 852: Adjust C1 to obtain same gain at 100 KHz as at 1 KHz (within ± 0.5 dB)

c. Gain Adjustment

This adjustment may be performed if the passband gain, or the attenuation at the cutoff frequency is determined to be out of specification. Connect the 5100 Frequency Synthesizer to the input of the instrument and the 400FL AC Voltmeter to the appropriate points indicated below. Proceed as follows:

^{*} The Frequency Synthesizer should be terminated with 50 ohms and the Filter Channel under adjustment should be terminated with 5K.

Model 452

1. Set filter settings as follows:

 5.00×100

Lo Pass

0 dB Gain

Flat Amplitude

- 2. Set input frequency to 500 Hz. Connect the AC Voltmeter to TP-1 and adjust input amplitude to obtain a reading of -10.0 dBV.
- 3. Move the AC Voltmeter to TP-2 and verify a reading of -14.1 dBV (\pm 0.1 dB).
- 4. Move the AC Voltmeter to OUT and adjust R19 to obtain a reading of -4.8 dBV.
- 5. Change filter setting to $5.00 \times 1K$ and adjust R11 to obtain a reading of -1.8 dBV at OUT.

Model 852

1. Set filter settings as follows:

 5.00×100

Lo Pass

0 dB Gain

Flat Amplitude

- 2. Set input frequency to 500 Hz. Connect the AC Voltmeter to TP-1 and adjust input amplitude to obtain a reading of -10.0 dBV.
- 3. Move the AC Voltmeter to TP-2 and verify a reading of -15.5 dBV (\pm 0.1 dB).
- 4. Move the AC Voltmeter to TP-3 and adjust R19 to obtain a reading of -17.4 dBV.
- 5. Move the AC Voltmeter to TP-4 and adjust R24 to obtain a reading of -12.8 dBV.
- 6. Move the AC Voltmeter to OUT and adjust R31 to obtain a reading of +3.6 dBV.
- 7. Change filter setting to $5.00 \times 1K$ and adjust R11 to obtain a reading of +6.6 dBV at OUT.
- d. High Frequency (x 10K) Cutoff Adjustment

This adjustment may be performed if cutoff frequency in the x 10K position is determined to be out of specification, while other positions are within specification. It should also be performed if the Gain adjustment described above has been performed. Connect the Frequency Synthesizer to the input of the instrument and the Gain/Phase meter to the appropriate points shown below. Use the following settings:

	<u>A</u>	<u>B</u>	<u>C</u>
Input Frequency :	50.0 KHz	100.0 KHz	50.0 KHz
Amplitude :	1.0 V rms	1.0 V rms	1.0 V rms
Filter Settings :	5.00 x 10K	1.00 x 10K	5.00 x 10K
	Lo Pass	Hi Pass	Hi Pass
	0 dB Gain	0 dB Gain	0 dB Gain
	Flat Amplitude	Flat Amplitude	Flat Amplitude

Model 452:	Perform	the	following	adjustments:
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Gain/Phase meter connected between:	TP-1 & TP-2	TP-2 & OUT	IN & OUT
A - Alternately adjust:	C29 & C34	C39 & C44	C39 & C44
to obtain Gain (dB): and Phase (deg):	-4.1 ± 0.2 90 ± 1	+9.3 ± 0.2 90 ± 3	-3.0 ± 0.2 180 ± 4
B – Adjust: to obtain Gain (dB):			R16 0.0 + 0.1
C – Adjust: to obtain Gain (dB):			R21 -3.0 ± 0.0

Model 852: Perform the following adjustments:

Gain/Phase met		TP-2 & TP-3	TP-3 & TP-4	TP-4 & OUT	IN & OUT
A - Alternately	Adjust: C29 & C	C34 C39 & C4	4 C49 & C5	C59 & C64	C59 & C64
to obtain Go	in (dB): -5.5 ± 0).2 -1.9 ± 0.	2 +4.6 ± 0.	$2 + 16.5 \pm 0.$	2 -3.0 ± 0.5
& Phase (deg): 90 ± 1	90 ± 1	90 ± 2	90 ± 6	180 ± 8

 \underline{B} - Adjust:

to obtain Gain (dB): 0 + 0.2

<u>C</u> - Adjust:

to obtain Gain (dB): -3.0 ± 0.0

4-5. TROUBLESHOOTING PROCEDURES

a. 1st Level Troubleshooting

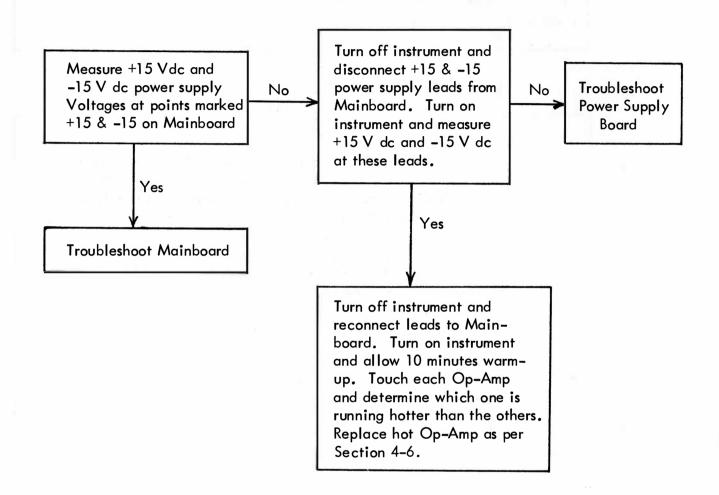
If both LED indicators fail to operate when the power switch is in the ON position:

- 1. Make certain that line power is available to the instrument.
- 2. Check that the 115/230 volt switch is in proper position for the available line voltage.
- 3. Check the fuse and replace, if defective.
- 4. With the power switch in the ON position check continuity of the power cord with an ohmmeter.
- 5. Check proper functioning of the Floating Operation switch by verifying a short/open between the third wire of the power cord and the shell of one of the BNC connectors.

If one LED indicator is on and the other is off, troubleshoot the Power Supply board (see 3rd Level Troubleshooting).

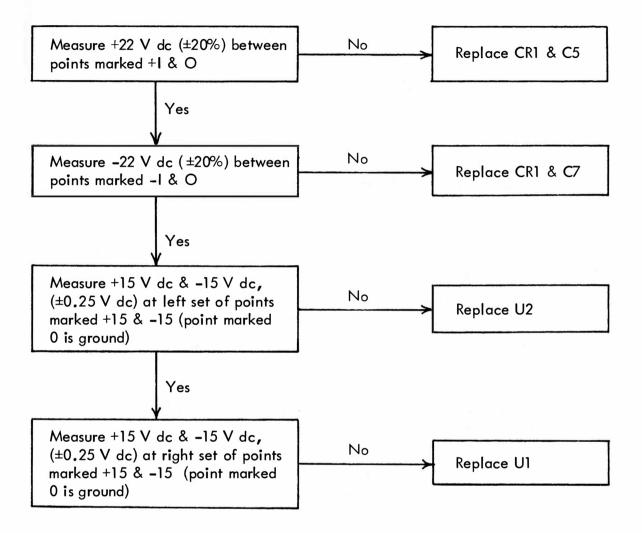
b. 2nd Level Troubleshooting

- If both indicators are on but the instrument fails to operate, remove the hardware that secures the top and bottom covers to the rear panel; slide back and remove top and bottom covers.
- 2. Perform the procedure in the order given in the 2nd Level Troubleshooting Tree. Voltages (±0.25 Volts) given in this Tree are measured with respect to ground using a Digital Multimeter (See Section 4–2. for Recommended Test Equipment).



c. 3rd Level Troubleshooting: Power Supply Board

- 1. To gain access to the Power Supply board, proceed as follows:
 - a. Remove the two screws which fasten the Rear Panel to the Side Frames and pull back the Rear Panel.
 - b. Remove the two screws which fasten the Power Supply Shield Box to the Rear Panel and move the Shield Box forward.
 - c. Remove the four screws which fasten the Power Supply board to the Rear Panel standoffs. Disconnect Power Supply leads from Mainboards and move Power Supply board out of the Shield Box.
- 2. Perform the procedure in the order given in the 3rd Level Trouble-shooting Tree. Voltages given in this Tree are measured with respect to ground using a Digital Multimter (See Section 4-2. for Recommended Test Equipment).
- 3. Repair as per Section 4–6. and replace by reversing the previous procedure.

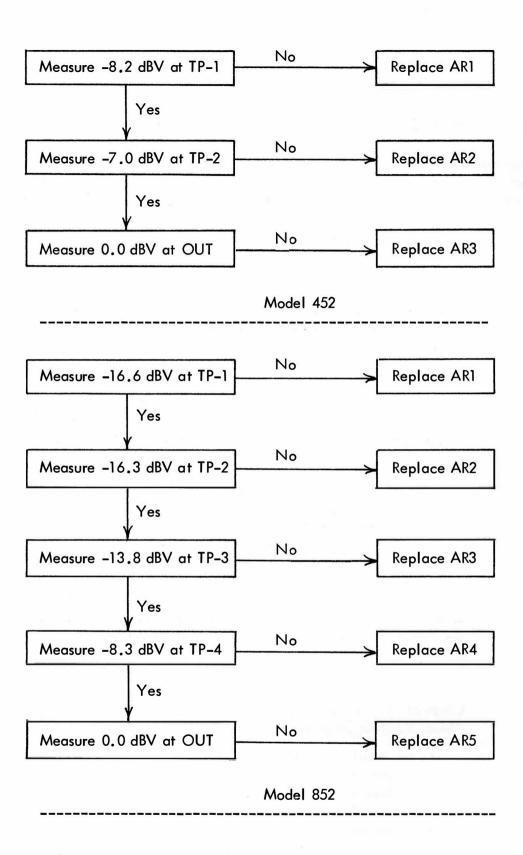


d. 4th Level Troubleshooting: Mainboard

1. Set filter channel controls as follows:

5.00 x 1K Lo Pass 0 dB Gain Flat Amplitude

- 2. Apply input signal at 500 Hz and adjust its amplitude to 0.0 dBV.
- 3. Perform the procedure in the order given in the 4th Level Trouble-shooting Tree. Voltages (±0.2 dB) given in this Tree are measured with respect to ground using an AC Voltmeter (See Section 4-2. for Recommended Test Equipment).
- 4. If replacement of any component is required, access to the bottom of the Mainboard is either readily available, or, if behind one of the Support Bars, it may be made available as follows:
 - a. Remove the three screws from each Mainboard that fasten them to the Support Bar.
 - b. Remove all fastening nuts from the Shield Board (between channels) and lift Shield Board supporting lugs out of the holes in Support Bars.
 - c. Remove the two screws which fasten the Support Bar to the Side Frames. Lift Mainboards slightly and slide Support Bar forwards (or backwards) to expose desired area on bottom of Mainboard.
 - d. Repair as per Section 4-6. and replace by reversing the above procedure.



4th Level Troubleshooting Tree: Mainboard

4-6. PRINTED CIRCUIT BOARD REPAIR

When replacing integrated circuits or other electronic components soldered to printed-circuit boards, the procedures indicated below should be followed to prevent potential damage to the board.

- 1. Determine by toubleshooting techniques, which component has failed.
- 2. Remove the defective component from the board by cutting the pins or leads with a small diagonal clipping tool. (Always remove and replace the entire component.)
- 3. Apply heat (40-50 W soldering iron) sparingly to each of the cut pins or leads and remove from the board; clean the hole (s) with a toothpick or solder suction tool.
- 4. Form the tinned leads of the replacement part and insert in the printed circuit holes; solder, then trim leads to extend 1/16-inch beyond the back surface of the board. (Use only 63-37 solder with maximum 1/16-inch diameter.)
- 5. When soldering semiconductor devices and all small components, be sure to use a heat sink tool or long-nosed plier connected to the component lead (s) while each is being soldered. Allow the soldered connection to cool before removing the heat sink.
- 6. Clean all dirt and solder-flux from the printed circuit traces by liberal application of isopropyl alcohol or freon-type solvents.

SECTION V

REPLACEABLE PARTS LISTS & DIAGRAMS

5-1. INTRODUCTION

This section contains an alphanumeric listing of all replaceable electrical parts used in the instrument. Reference designations applying to the parts list are provided below. Component-location and schematic diagrams are also included.

5-2. ORDERING INFORMATION

To order replacement parts, address your order to:

Rockland Systems Corporation 230 West Nyack Road West Nyack, New York 10994

Specify the following information:

- 1) Model and serial number of instrument
- 2) Circuit reference designation
- 3) Rockland part number
- 4) Description of part

REFERENCE DESIGNATIONS

Α	Assembly	MP	Mechanical Part
AR	Amplifier	Р	Plug
В	Motor	Q	Transistor
C	Capacitor	R	Resistor
CR	Diode	S	Switch
DS	Device Indicator	T	Transformer
F	Fuse	U	Microcircuit
FL	Filter	VR	Voltage Regulator
J	Conncector	X	Socket
K	Relay		

ASSEMBLY A1

Power Supply Assembly, Models 452 & 852

Ref. Des.	Description	P/N
C1, C2, C3 C5, C7 C6, C8, C11, C12 C9, C10, C13, C14	C: Fxd cer 0.01 uF +80 -20% 100 V C: Fxd elect 500 uF 50 V C: Fxd tant 0.01 uF 20% 35 V C: Fxd polyester 0.0015 uF 10% 100 V	100-3100 109-7500 109-4100 105-2150
CR1	CR: Sil FWB 50 PIV 1.5 A	130-0140
R1, R2 R3, R4, R5, R6 R7, R8	R: Fxd comp 15K 5% 1/4W R: Fxd comp 10 ohm 5% 1/4W R: Fxd comp 2.2K 5% 1/4W	116-3151 116-0101 116-2221
S1 S2	S: Switch Slide DPDT, PC 115/230 S: Switch Slide DPDT, PC Mount	342-2203 342-2202
TI	T: Transformer, Power	177-3012
U1, U2	U: Dual volt reg ±15 V 100 mA	120-0152

ASSEMBLY A2, A3

Mainboard Assembly, Model 452

C1 C:	Var mica 2-25pF 175 V	108-0250
	Fxd mica dipped 100pF 10% 500 V	101-1100
C10, C12, C13 C4, C6, C15, C16 C8 C11 C14 C25, C30, C35, C40 C26, C31, C36, C41 C27, C32, C37, C42 C28, C33, C38, C43 C5	Fxd ceram. 0.01uF +80 -20% 30 V Fxd tant 1uF 20% 35 V Fxd mica dipped 33pF 10% 500 V Fxd mica dipped 200pF 10% 500 V Fxd mica dipped 47pF 10% 500 V Fxd polycarb 1.0uF 1% 100 V Fxd polycarb 0.1uF 1% 100 V Fxd polycarb 0.01uF 1% 100 V Fxd mica dipped 820pF 10% 500 V Var mica 24-200pF 175 V	100-3101 109-5100 101-0330 101-1200 101-0470 104-5100 104-4100 104-3100 101-1820 108-1200
	R: Zener 6.8 V 10% 400 mW R: Sil low leak 70 PIV 200 mA	131 - 9680 132 - 0457
R1 R: R2, R3 R: R4 R: R5, R6 R: R7, R24 R: R8, R23 R: R9, R13, R17 R: R10 R: R11, R19 R: R12 R: R14 R: R15, R25 R: R16, R21 R: R20 R: R22 R: R22 (Option-02) R: R26, R18 R: R27 * R: R28 * R: R29 * R:	Fxd metflm 100K 1% 1/8W Fxd comp 2.7K 5% 1/4W Fxd comp 10K 5% 1/4W Fxd metflm 200K 1% 1/4W Var cermet 200K 10% 1/2W Fxd comp 100 ohm 5% 1/4W Fxd metflm 4.32K 1% 1/8W Var cermet 50 ohm 10% 1/2W Fxd metflm 1.5K 1% 1/8W Fxd metflm 1.5K 1% 1/8W Fxd metflm 1.0K 1% 1/8W Var cermet 10K 10% 1/2W	113-9000 113-1000 116-2271 116-3101 113-2000 118-4201 116-1101 111-4320 118-0500 111-1500 110-1540 111-1000 118-3101 111-2000 116-0471 116-1621 111-2490 116-2101 116-3331 116-3471

^{*} Factory selected value; typical value shown

ASSEMBLY A2, A3 - continued

Mainboard Assembly, Model 452

Ref. Des.	De	scription	P/N
R41, R45, R65, R69 R42, R46, R66, R70 R43, R47, R67, R71 R44, R48, R68, R72 R49, R53, R73, R77 R50, R54, R74, R78 R51, R55, R75, R79 R52, R56, R76, R80 R57, R61, R81, R85 R58, R62, R82, R86 R59, R63, R83, R87	R: R: R: R: R: R:	Fxd metflm 1.99K 1% 1/8W Fxd metflm 7.96K 1% 1/8W Fxd metflm 15.9K 1% 1/8W Fxd metflm 3.98K 1% 1/8W Fxd metflm 19.9K 1% 1/8W Fxd metflm 79.6K 1% 1/8W Fxd metflm 159K 1% 1/8W Fxd metflm 39.8K 1% 1/8W Fxd metflm 199K 1% 1/8W Fxd metflm 796K 1% 1/8W Fxd metflm 796K 1% 1/8W Fxd metflm 796K 1% 1/8W Fxd metflm 1.59M 1% 1/8W	111-1990 111-7960 112-1590 111-3980 112-1990 112-7960 113-1590 112-3980 113-1990 113-7960 114-1590
R60, R64, R84, R88 S1, S9 S2, S3, S4 S5, S6 S8 AR1, AR2, AR3	S: S: S: S:	Push button Push/Push DPDT Rotary 4 pole 12 pos BCD Coded Push button Push/Push 8PDT Rotary 7 pole 2–5 pos Linear Op-Amp	113-3980 341-2202 345-4120 341-8200 343-7051 120-1007
		Fxd mica dipped 100pF 10% 500V ASSEMBLY A4, A5 n -01 Assembly, Model 452 P/N 004-0980	101-1100
Ref. Des. C1, C2, C3, C4	C: Fx	Description d polycarb 10uF 1% 100V	<u>P/N</u> 104-6100

ASSEMBLY A2, A3

Mainboard Assembly, Model 852

Ref. Des.		Description	P/N
C1 C2, C8, C14 C3, C5, C7, C9, C10, C12, C13, C15, C16,		Var mica 2–25pF 175 V Fxd mica dipped 100pF 10% 500 V	108-0250 101-1100
C18, C19 C4, C6, C21, C22 C11 C17 C20, C23	C: C: C: C:	Fxd ceram. 0.01 uF +80 -20% 30 V Fxd tant 1uF 20% 35 V Fxd mica dipped 500pF 10% 500 V Fxd mica dipped 47pF 10% 500 V Fxd mica dipped 22pF 10% 500 V	100-3101 109-5100 101-1500 101-0470 101-0220
C25, C30, C35, C40, C45, C50, C55, C60 C26, C31, C36, C41, C46, C51, C56, C61	C: C:	Fxd polycarb 1.0uF 1% 100 V Fxd polycarb 0.1uF 1% 100 V	104-5100 104-4100
C27, C32, C37, C42, C47, C52, C57, C62 C28, C33, C38, C43, C48, C53, C58, C63	C:	Fxd polycarb 0.01 uF 1% 100 V Fxd mica dipped 820pF 10% 500 V	104-3100 101-1820
C49, C33, C39, C63 C29, C34, C39, C44, C49, C54, C59, C64 C67	C:	Var mica 24–200pF 175 V Fxd ceram . 1000pF +80 –20% 1000 V	108-1200 100-2100
CR1, CR4 CR2, CR3		Zener 6.8 V 10% 400 mW Sil low leak 70 PIV 200 mW	131 - 9680 132 - 0457
R1 R2, R3 R4 R5, R6 R9, R13, R17, R22, R29 R10 R11, R19, R24, R31 R12, R20, R25, R32, R38	R: R: R: R: R: R: R:	Fxd metflm 900K 1% 1/8W Fxd metflm 100K 1% 1/8W Fxd comp 4.7K 5% 1/4W Fxd comp 10K 5% 1/4W Fxd comp 100 ohm 5% 1/4W Fxd metflm 453 ohm 1% 1/8W Var cermet 50 ohm 10% 1/2W Fxd metflm 1.0K 1% 1/8W	113-9000 113-1000 116-2471 116-3101 116-1101 110-4530 118-0500 111-1000

^{*} Factory selected value; typical value shown

ASSEMBLY A2, A3 - continued

Mainboard Assembly, Model 852

Ref. Des.		Description	P/N
D1.4		F 1 20 57 (1 20 2 (0))	
R14	R:	Fxd metflm 57.6 ohm 1% 1/8W	119-5760
R15, R35 R16	R: R:	Fxd metflm 1.5K 1% 1/8W Var cermet 1K 10% 1/2W	111 <i>-</i> 1500 118 <i>-</i> 2102
R18	R:	Fxd metflm 340 ohm 1% 1/8W	110-2102
R23	R:	Fxd metflm 887 ohm 1% 1/8W	110-3400
R27, R8	R:	Var cermet 200K 10% 1/2W	118-4201
R28, R7	R:	Fxd metfIm 200K 1% 1/8W	113-2000
R30	R:	Fxd metflm 1.62K 1% 1/8W	111-1620
R33	R:	Var cermet 10K 10% 1/2W	118-3101
R34	R:	Fxd metflm 1.33K 1% 1/8W	111-1330
R36	R:	Fxd comp 47 ohm 5% 1/4W	116-0471
R36 (Option-02)	R:	Fxd comp 620 ohm 5% 1/4W	116-1621
R37 *	R:	Fxd comp 5.6K 5% 1/4W	116-2561
R41, R45, R65, R69,			
R89, R93, R113, R117	R:	Fxd metflm 1.99K 1% 1/8W	111-1990
R42, R46, F66, F70,			
R90, R94, R114, F118	R:	Fxd metflm 7.96K 1% 1/8W	111 <i>-</i> 7960
R43, R47, R67, R71,	D	F 15 OK 10/ 1 /0W	110 1500
R91, R95, R115, F119 R44, R48, R68, R72,	R:	Fxd metflm 15.9K 1% 1/8W	112-1590
R92, R96, R116, R120	R:	Fxd metflm 3.98K 1% 1/8W	111 -3980
R49, R53, R73, R77,	N;	1 Xd me11m 3.76K 17c 176W	111-3900
R97, R101, R121, R125	R:	Fxd metflm 19.9K 1% 1/8W	112-1990
R50, R54, R74, R78,	• • • •	7 x x x x x x x x x x x x x x x x x x x	112-1770
R98, R102, R122, R126	R:	Fxd metflm 79.6K 1% 1/8W	112-7960
R51, R55, R75, F79,		, ,	
R99, R103, R123, R127	R:	Fxd metflm 159K 1% 1/8W	113-1590
R52, R56, R76, R80,			
R100, R104, R124, R128	R:	Fxd metflm 39.8K 1% 1/8W	112-3980
R57, R61, R81, R85,			
R105, R109, R129, R133	R:	Fxd metflm 199K 1% 1/8W	113-1990
R58, R62, R82, R86,	_		
R106, R110, R130, R134	R:	Fxd metflm 796K 1% 1/8W	113-7960
R59, R63, R83, R87,	ь	F (CL 1 5044.10/ 1 /44/	114 1500
	R:	Fxd metflm 1.59M 1% 1/4W	114-1590
R60, R64, R84, R86, R108, R112, R132, R136	R.	Fxd metflm 398K 1% 1/8W	112 2000
1100, 1112, 1102, 1100	IV;	1 Au mentin oron 170 170W	113-3980

^{*} Factory selected value: typical value shown

ASSEMBLY A2, A3 - continued

Mainboard Assembly, Model 852

P/N 004-0930

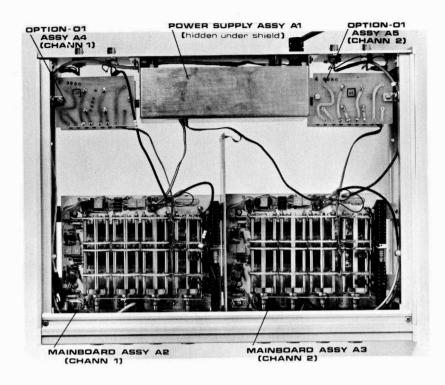
Ref. Des.		Description	P/N
R137* R140* R141*	R: R: R:	Fxd comp 330 ohm 5% 1/4W Fxd comp 3.9K 5% 1/4W Fxd comp 2.7K 5% 1/4W	116-1331 116-2391 116-2271
S1, S9 S2, S3, S4 S5, S6, S7 S8	S: S: S:	Push button Push/Push DPDT Rotary 8pole 12 pos Coded Push button Push/Push 8PDT Rotary 13 pole 2–5 pos	341 -2202 345-8124 341 -8200 344-3050
AR1, AR2, AR3 AR4, AR5	U:	Linear Op-Amp	120-1007
C65, C66 (Option-01 only)	C:	Fxd mica dipped 100pF 10% 500V	101-1100

ASSEMBLY A4, A5

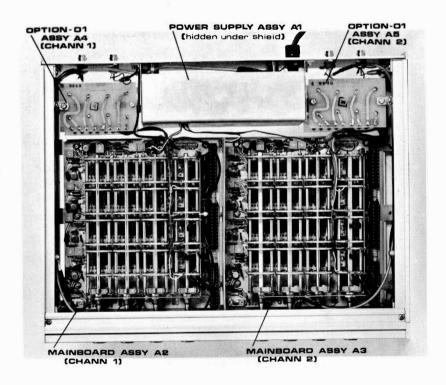
Option -01 Assembly, Model 852

Ref. Des.			Description	P/N
C1, C2, C3, C4, C5, C6, C7, C8	•	C:	Fxd polycarb 10uF 1% 100V	104-6100

^{*} Factory selected value; typical value shown



Model 452-01

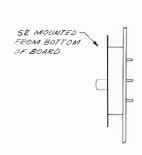


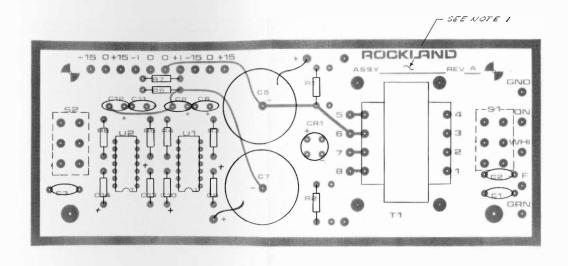
Model 852-01

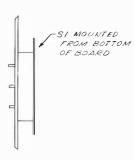
Fig. 5-1 Assembly Designation

COMPONENT - LOCATION &
SCHEMATIC DIAGRAMS

LTR	ECO NO.	CHANGED BY
A	RELEASE	July 20
C	272	D8 94/15

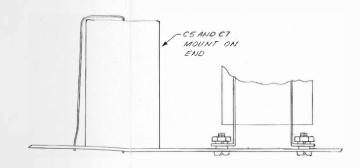






NOTES:

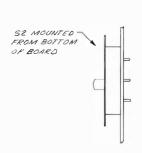
- 1) STAMP APPLICABLE ASSY No. AND USEABLE REV LETTER PER INK SPEC DWG No. 00-995-0001.
- 2) LEAD PROTRUSION THRU BOARD TO BE .062 MAX.
- 3) SHEET 2 IS "A" SIZE (L/M)

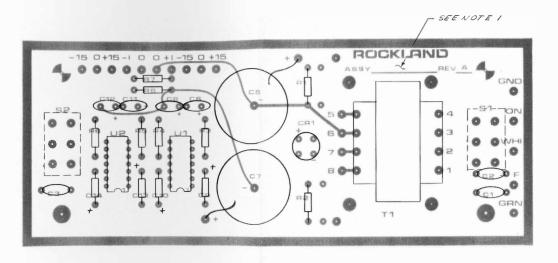


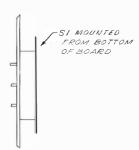
CHECKED BY:	/// 77:74	ROCKLA Rockland Systems Con
In Shanes	2-1-75	Confidential property of ROCKLA
MFG APPVL	3-29.25	not to be disclosed to others, repr any purpose except as authorized i
ALL DIMENSIONS AR	E IN	ASSEMBL POWER S

D 02 004-09

LTR	ECO NO.	CHANGED BY	APPV'D BY	Γ
A	RELEASE	J	SNT	2
C	272	D8 44/15	SNT	6.

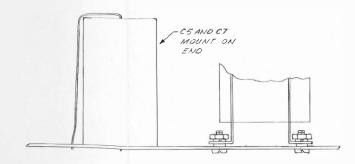






E5:

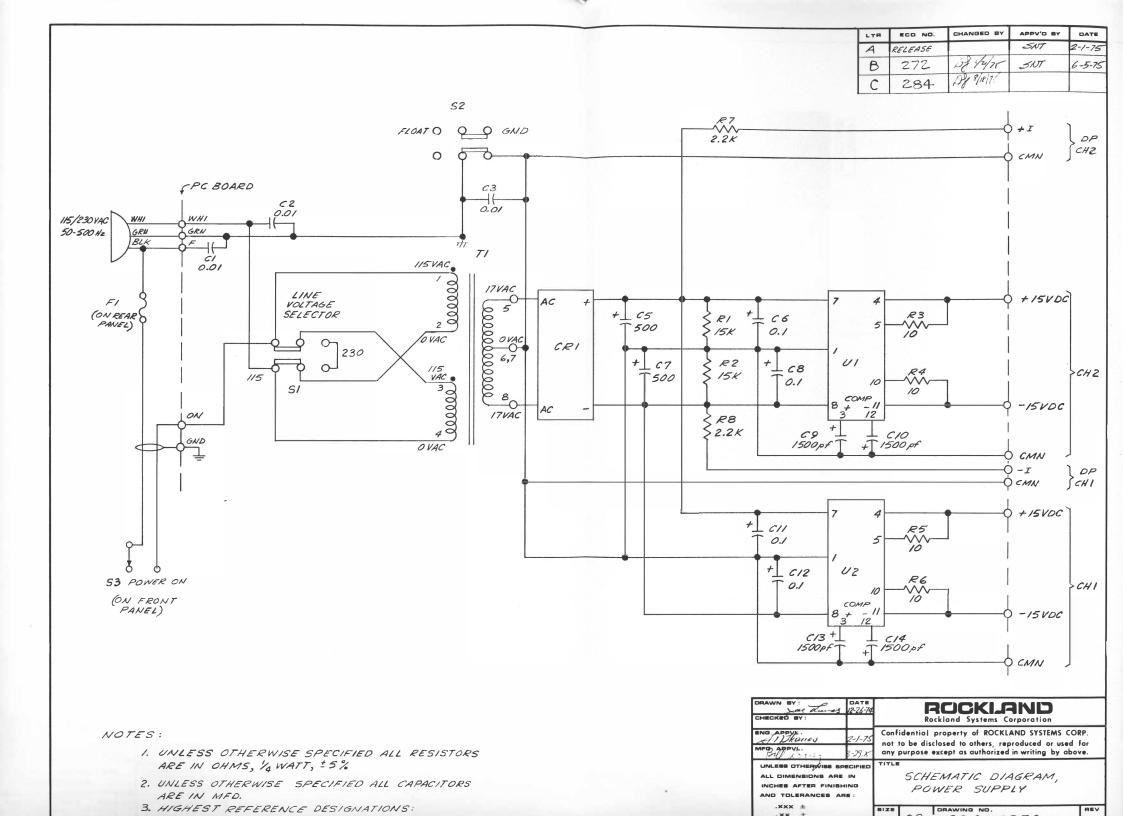
- 1) STAMP APPLICABLE ASSY No. AND USEABLE REV LETTER PER INK SPEC DWG No. 00-995-0001.
- 2) LEAD PROTRUSION THRU BOARD TO BE .062 MAX.
- 3) SHEET 2 IS "A" SIZE (L/M)



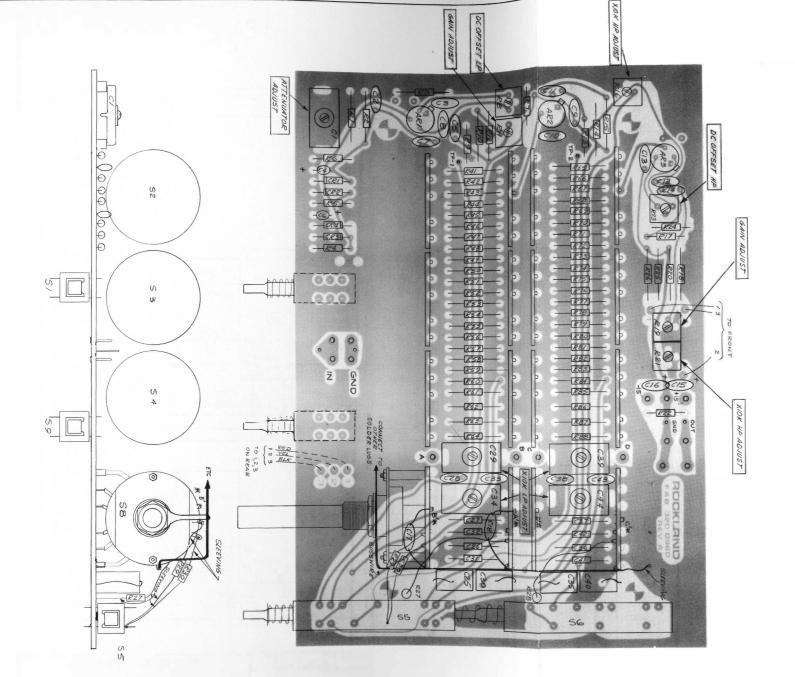
CHECKED BY:	CATE /221:79	ROCKLAND Rockland Systems Corporation
Shanes	2-1-75	Confidential property of ROCKLAND SYSTEMS Control to be disclosed to others, reproduced or uses
MEG APPVL.	3-29.25	any purpose except as authorized in writing by al
ALL DIMENSIONS ARE	IN IN	ASSEMBLY PCE
INCHES AFTER FINISH		POWER SUPPLY

D 02 004-0950

SCALE 2// SHEET / OF 2



LTR	ECO NO.	CHANGED BY	Ī
A	RELEASE	Yamay 9	
B	ECO 245	JOE LEWIS	
C	273	13 79/15	
D	285	De Block	



NOTES:

- 1) STAMP APPLICABLE ASSY No. USEABLE REV LETTER PER DWG No. 00-995-0001
- 2) LEAD PROTRUSION THRU BO TO BE .062 MAX
- 3) SHEET 2 IS A SIZE (UM)
- 4) * USED ON (-01) OPTION ONLY 000-0957, 000-0958, 0 000-0960, 000-0961

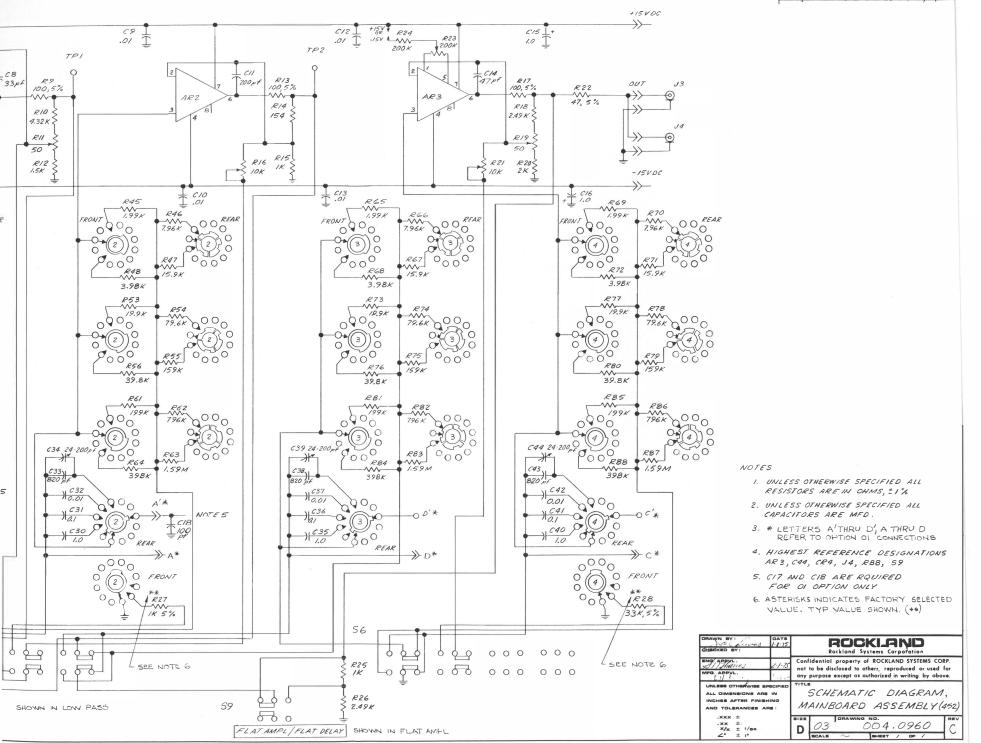
CRAWN BY: JOE LEWIS CHECKED BY:	PATE	ROCKLE
CHRICKED ST.		Rockland Systems Co
Manos	2-1-75	Confidential property of ROCKLI net to be disclosed to others, rep
MFG APBUL	30/25-	any purpose except as authorized
UNLESS OTHERWISE	SPECIFIED	TITLE
ALL DIMENSIONE A	R IN	ASSEMBLY P
AND TOLERANCES ARE:		MAINBOAR

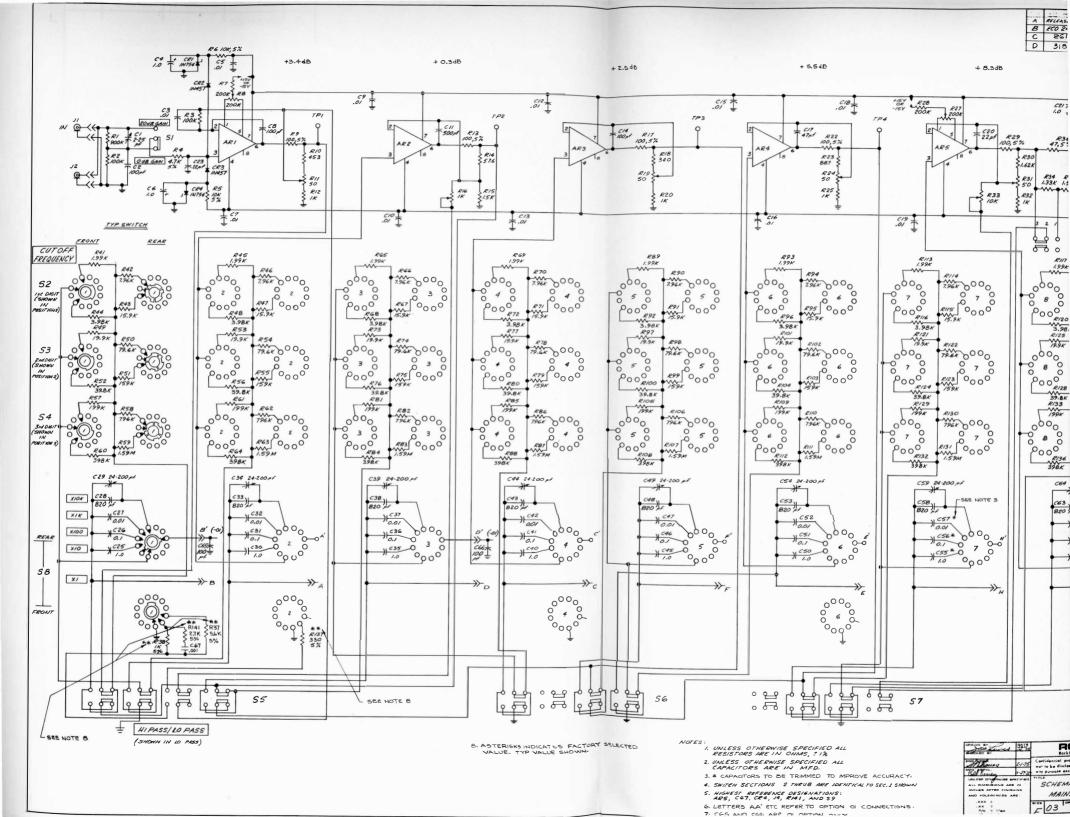
D 02 DRAWING NO D 004 - C

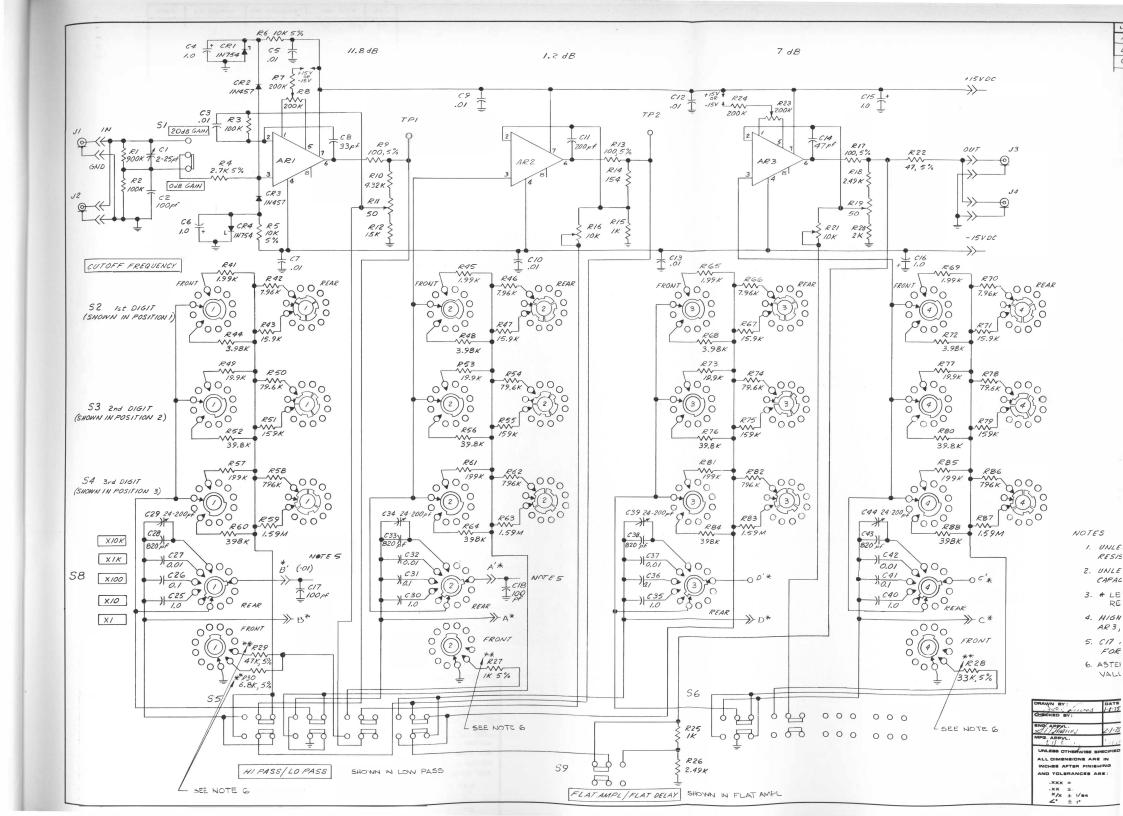
1.2 dB

7 dB

	LTR	ECO NO.	CHANGED BY	APPV'D BY	DA
	A	RELEASE	-	.547	2-1-
	B	ECO 245	JOE LEWIS	511	4-24
1	C	ECO 317	1.7 4/1/15	SIT AN	9-2

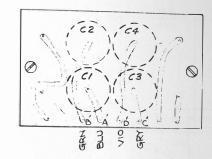




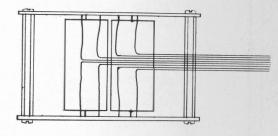


B RELEASED CHANGED BY APPYD BY DATE

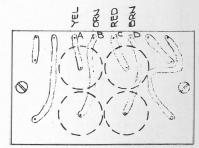
TOP VIEW



SIDE VIEW



BOTTOM VIEW



JOE LEWIS	W25/75	ROCKLAND
CHECKED BY:		Rockland Systems Corporation
M Thans	4/26/15	Confidential property of ROCKLAND SYSTEMS CORP. not to be disclosed to others, reproduced or used for
MFB POPUL.	1/28/25	any purpose except as authorized in writing by above.
//		TITLE

UNLESS OTHERWISE SPECIFIE
ALL DIMENSIONS ARE IN
INCHES AFTER FINISHING
AND TOLERANCES ARE:

TOLERANCES ARE:

XXX ±

X/X ± 1/84

Z' + 1'

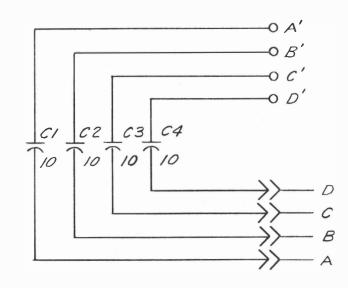
C SCALE

MULTIPLIER ASSEMBLY: 452 OPTION -OI

C 02 ORAWING NO. 004-0980

B

A RELEASED



CHECKED BY:

CHECKED BY:

ROCKIAND Systems Corporation

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UNLESS OTHERWISE SPECIFIED ALL DIMENSIONS ARE IN INCHES AFTER FINISHING AND TOLERANCES ARE:

AND TOLERANCES ARE:

SCALE

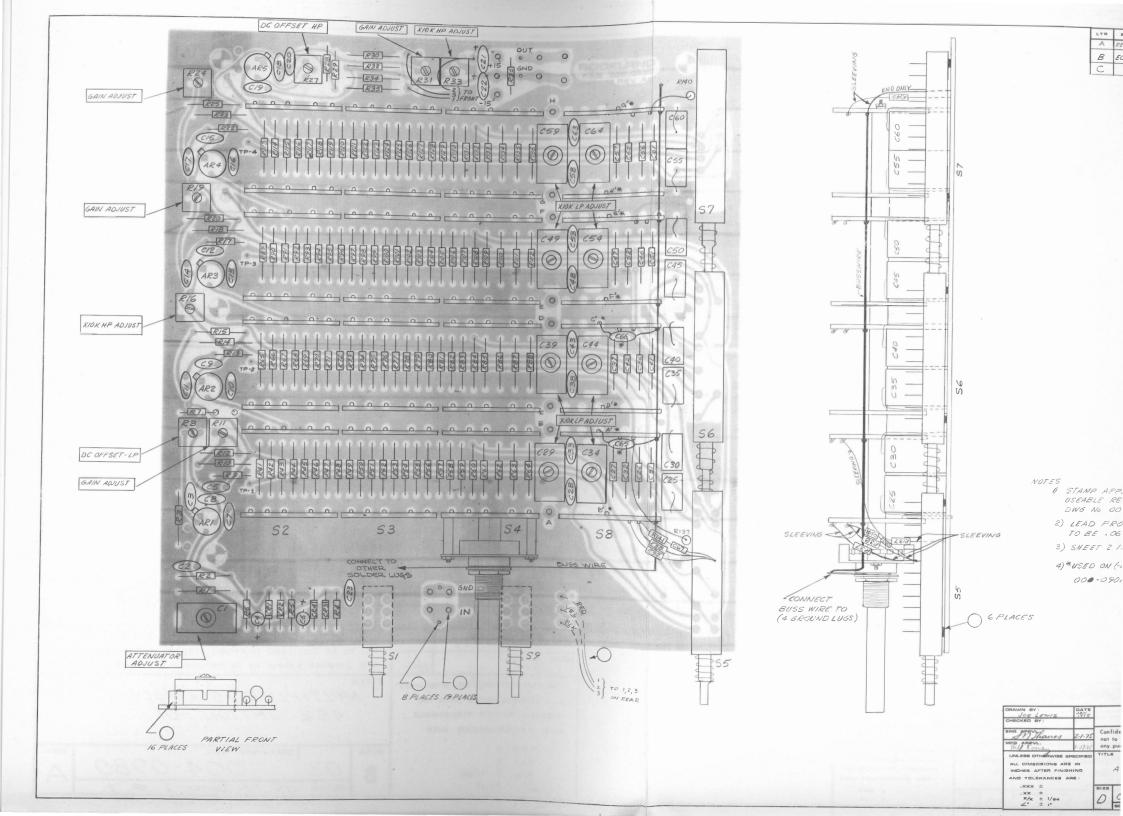
SIZE

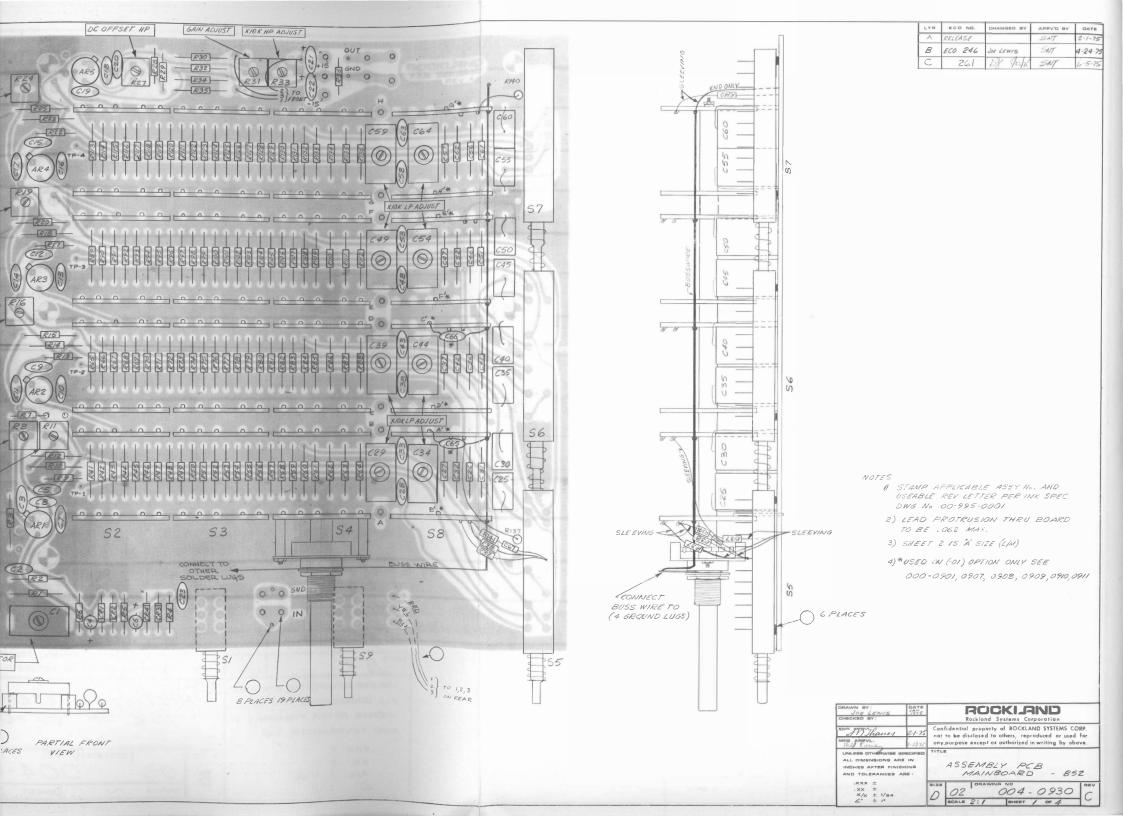
DRAWING NO.

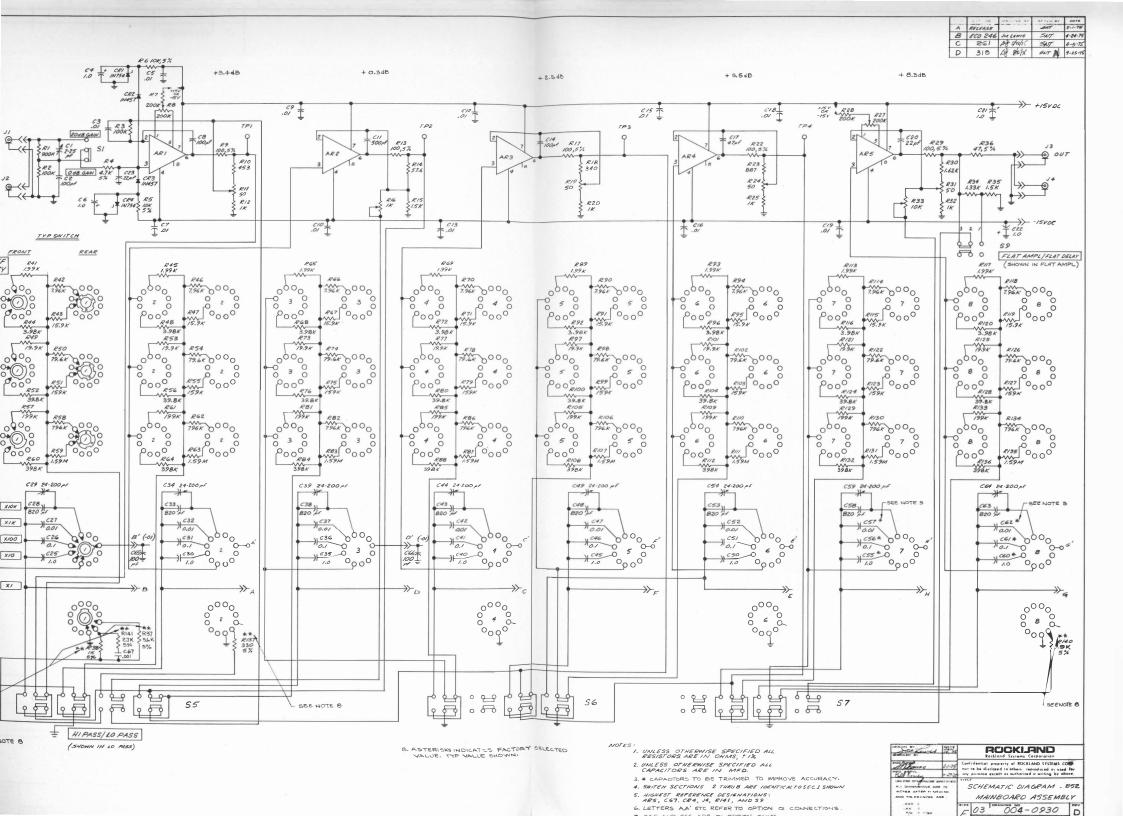
 $.xxx \pm$

.xx ± x/x ± 1/64 ∠° ± 1°

NOTE: CAPS IN MICROFARADS, ±1%

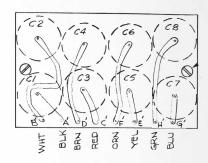




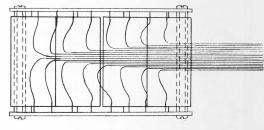


LTR ECO NO. CHANGED BY APPV'D BY DATE B RELEASED

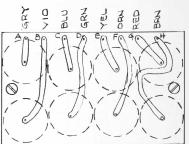
TOP VIEW



SIDE VIEW

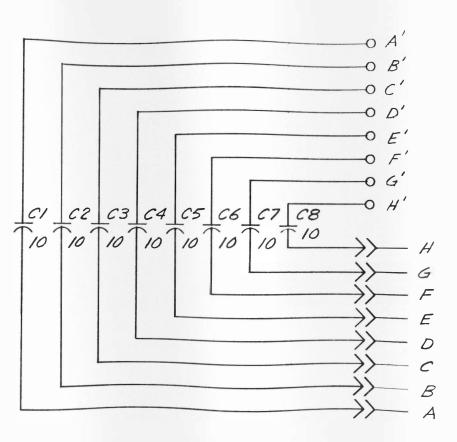


BOTTOM VIEW



DRAWN BY: Job LENYS CHECKED BY:	#/25/75	ROCKLAND Rockland Systems Corporation		
APPLATES 4/26/75 MFG APPLATES 4/26/75 MFG BJ KS Sur 4/26/75		Confidential property of ROCKLAND SYSTEMS CORP. not to be disclosed to others, reproduced or used for any purpose except as authorized in writing by above.		
UNLESS OTHERWISE S		MULTIPLIER ASSEMBLY:		
INCHES AFTER FINIS		852 OPTION -01		
.XXX ± .XX ± X/X ± 1/84		C 02 004-0940 REV		

A RELEASED



TE: CAPS IN MICROFARADS + 1%

CHECKED BY:	4/25/75	ROCKLAND Rockland Systems Corporation	
MFG APPVL.	4/26/15	Confidential property of ROCKLAND SYSTEMS CORI not to be disclosed to others, reproduced or used for any purpose except as authorized in writing by above	or
UNLESS OTHERWISE SE	ECIFIED	TITLE	
ALL DIMENSIONS ARE IN		MULTIPLIER ASSEMBLY:	
INCHES AFTER FINISH AND TOLERANCES AF		852 OPTION -01	
.xxx ± .xx ± x/ _x ± ¹/64 ∠° ± 1°		B 03 004-0940	REV